

Link Statistics of Dislocation Network during Strain Hardening

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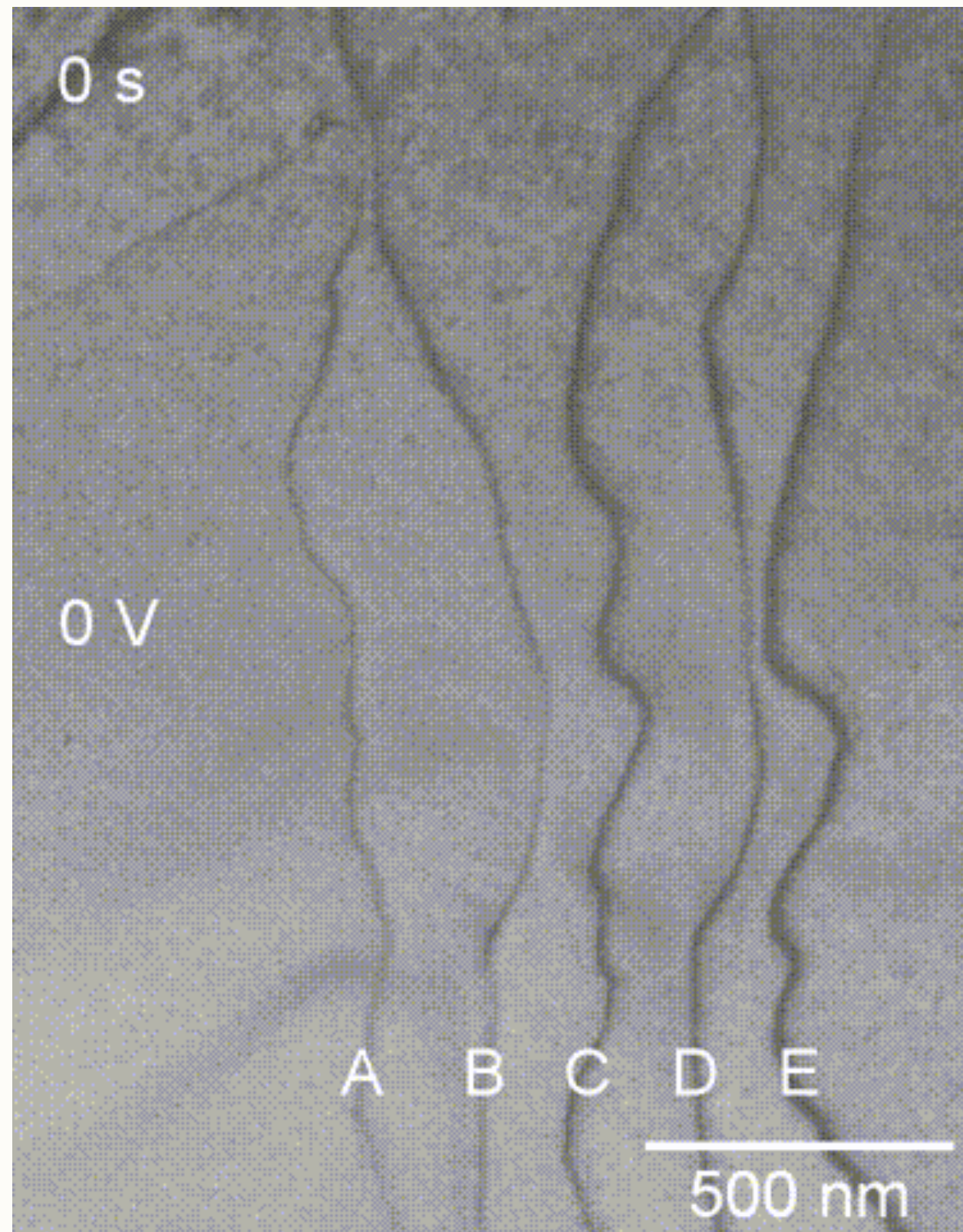
Alloys & Nuclear Materials:

Understanding evolution of defects

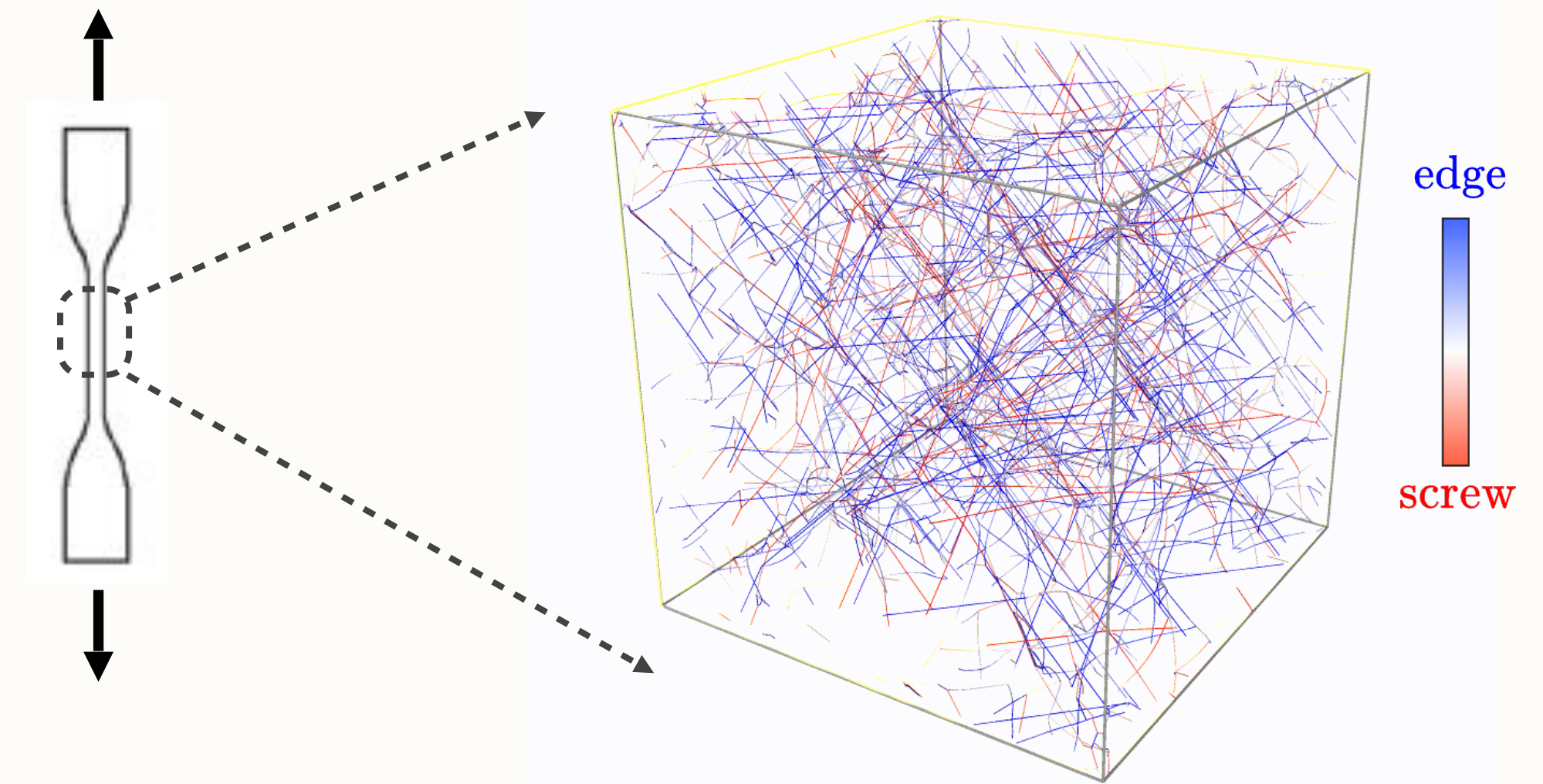
Dislocation dynamics controls plasticity

Dislocations are line **defects** in crystals

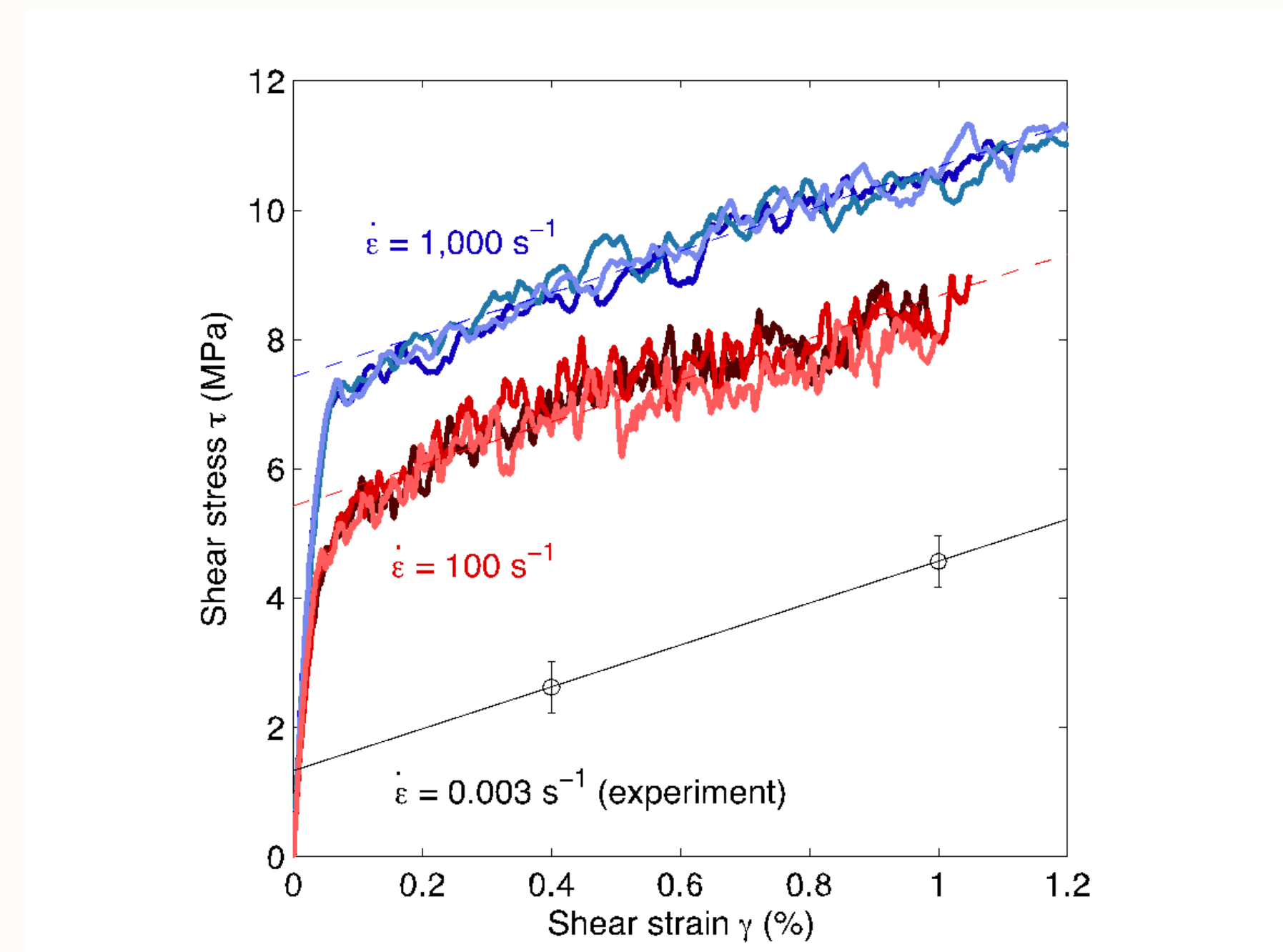
(Figure from experiment)



Li et al., *Nature Materials*, 2023



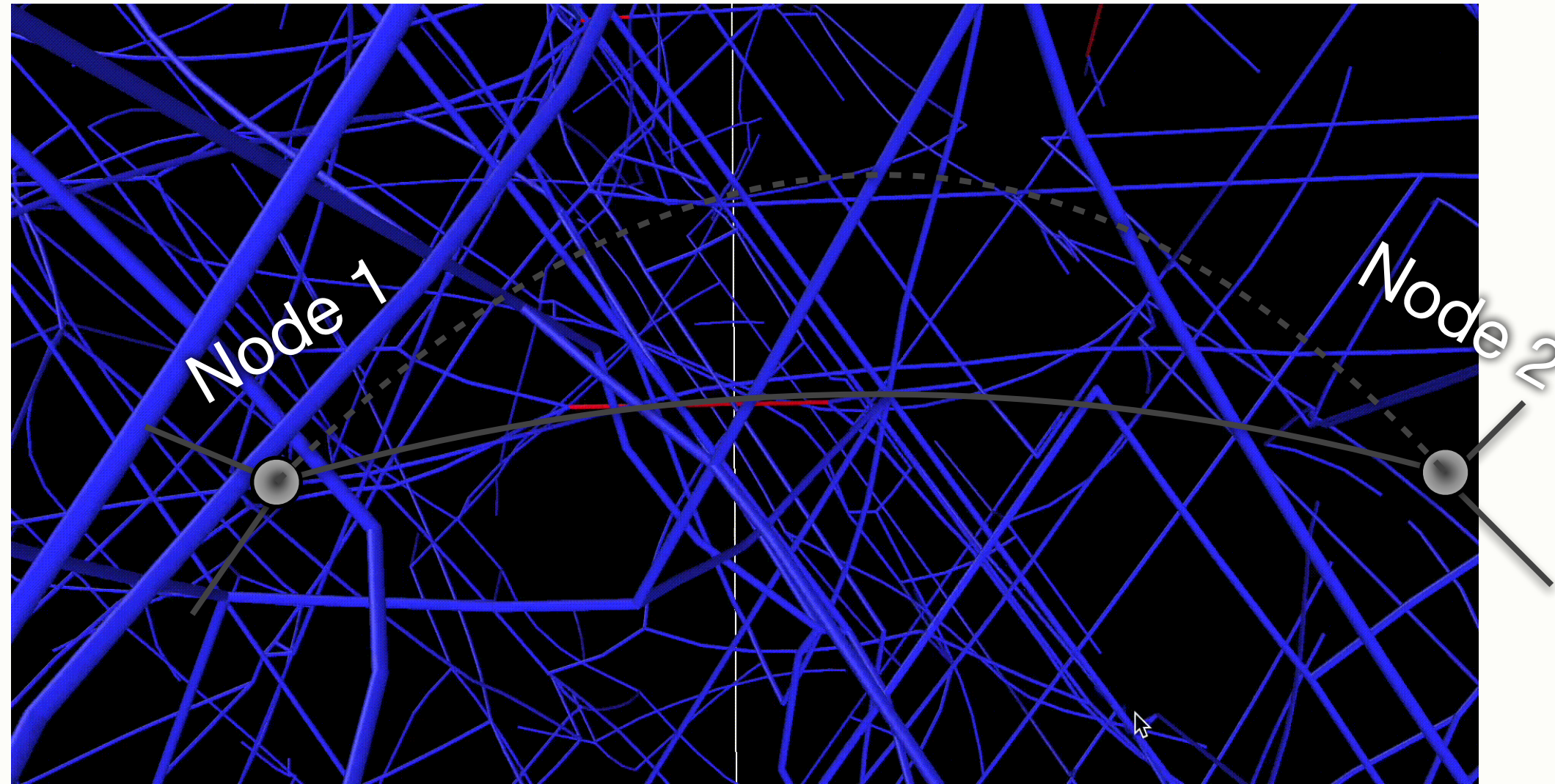
P: Lack of understanding of the **interactions** of the network (\leftrightarrow mechanical properties)!



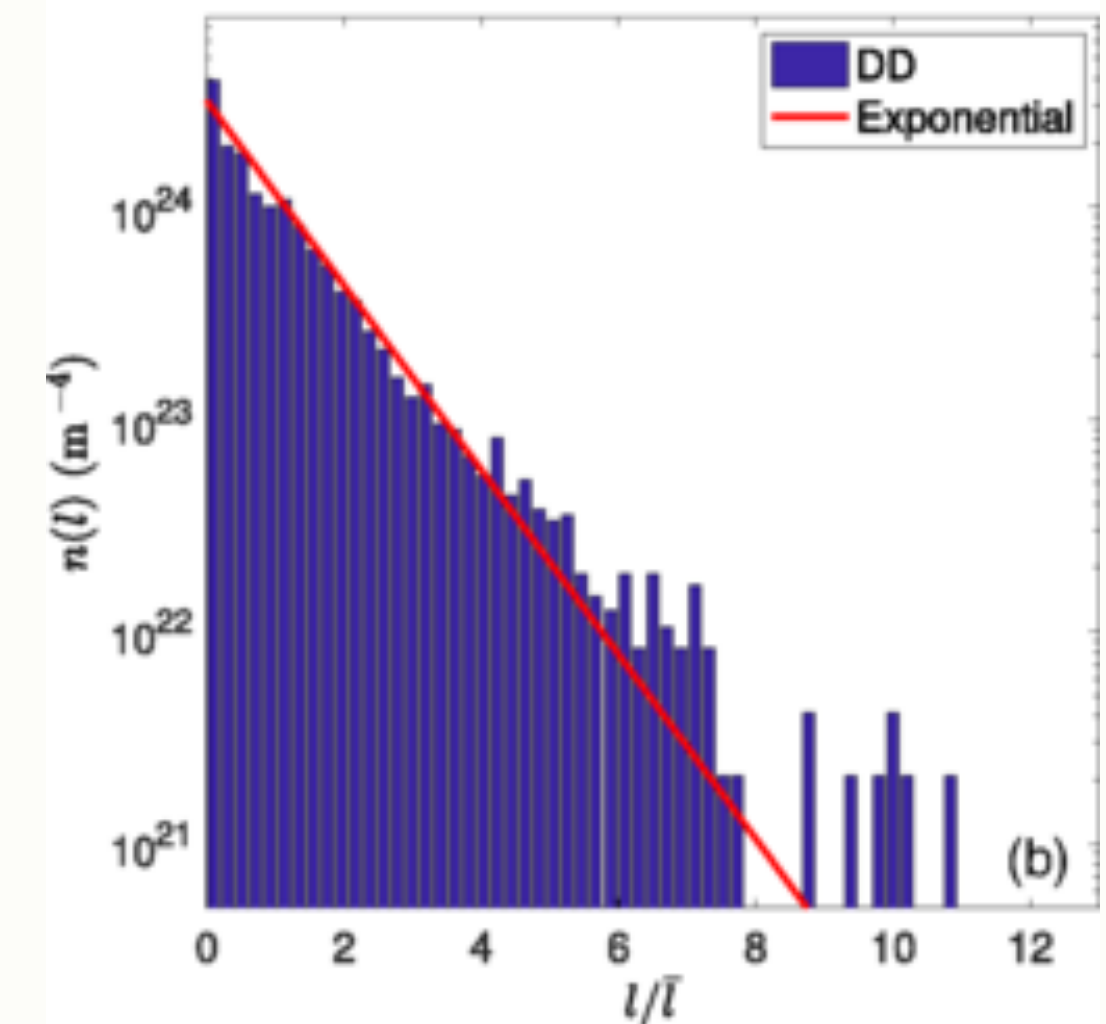
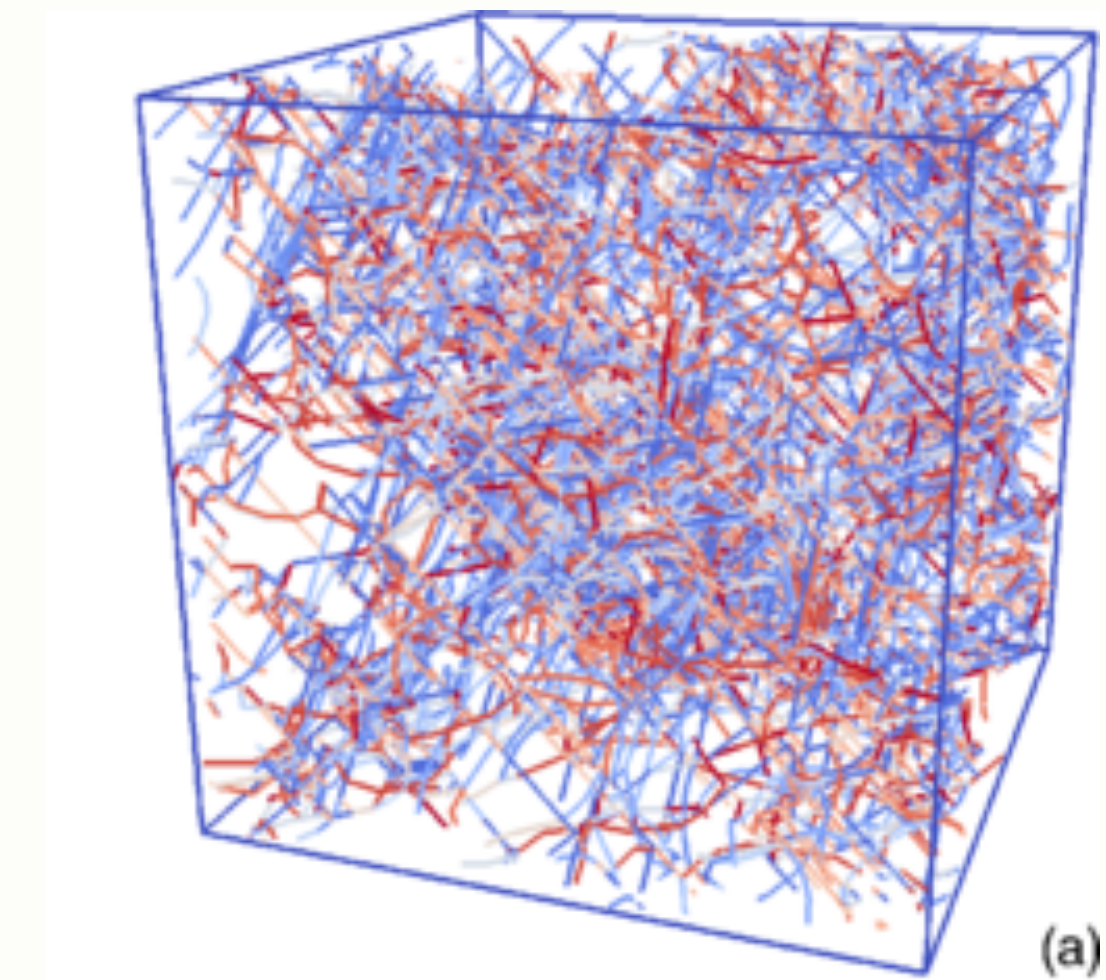
Sills et al., *Phys. Rev. Lett.*, 2018

Dislocation link lengths statistics: from *link* to *network*

[001] Loading on Cu



What is a link?




PHYSICAL REVIEW LETTERS **121**, 085501 (2018)

Dislocation Networks and the Microstructural Origin of Strain Hardening

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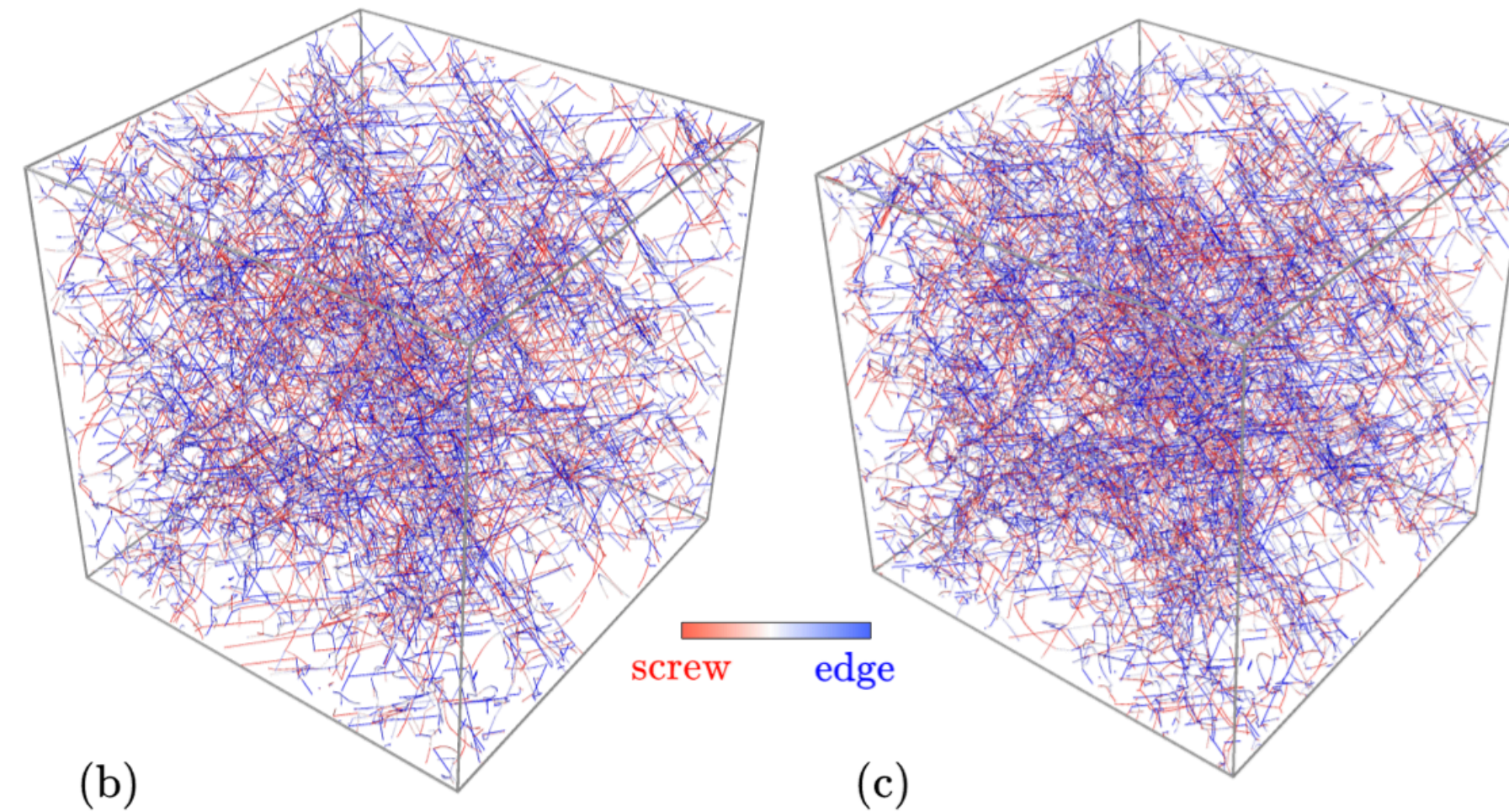
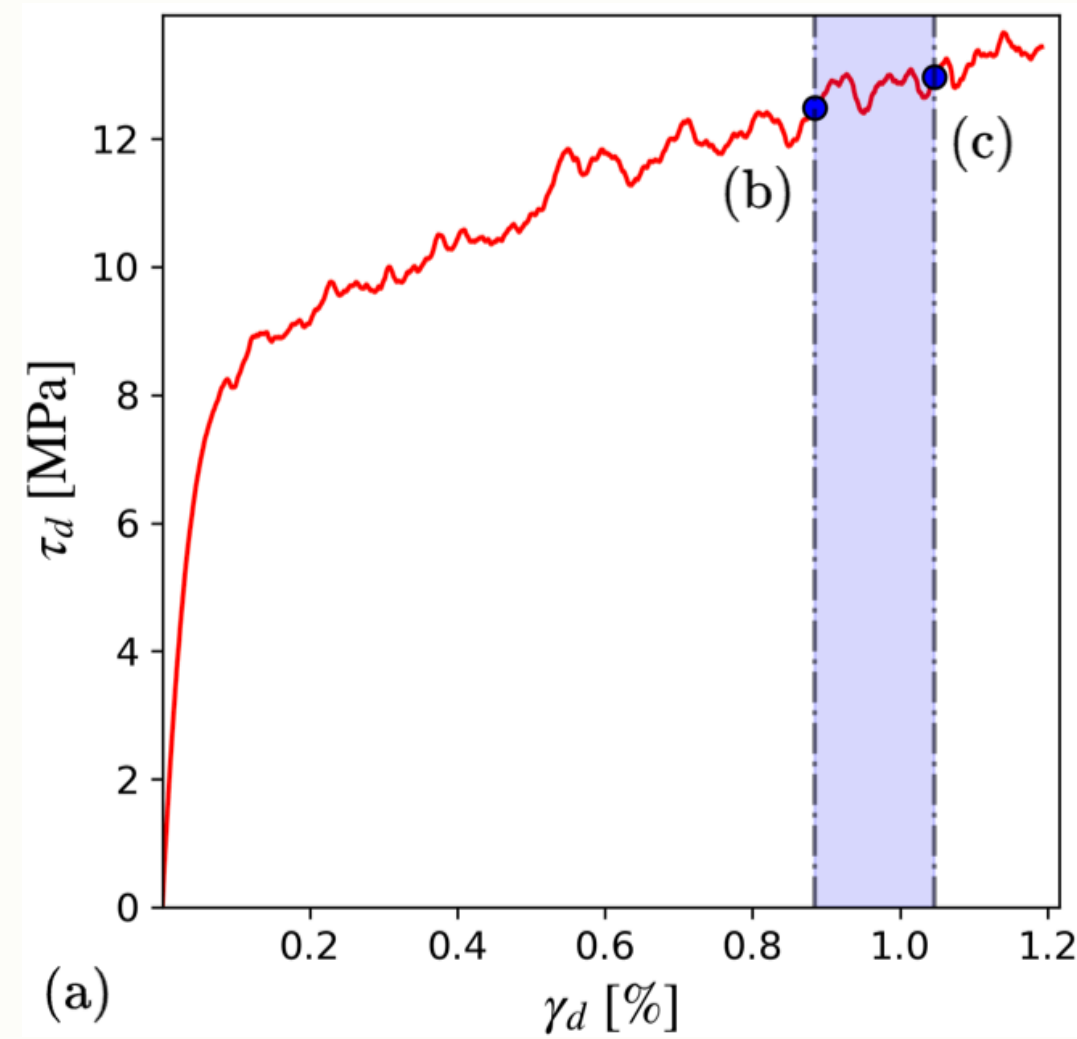
²Department of Mechanical Engineering, Stanford University, Stanford, California 94305, USA

 (Received 3 April 2018; published 20 August 2018)

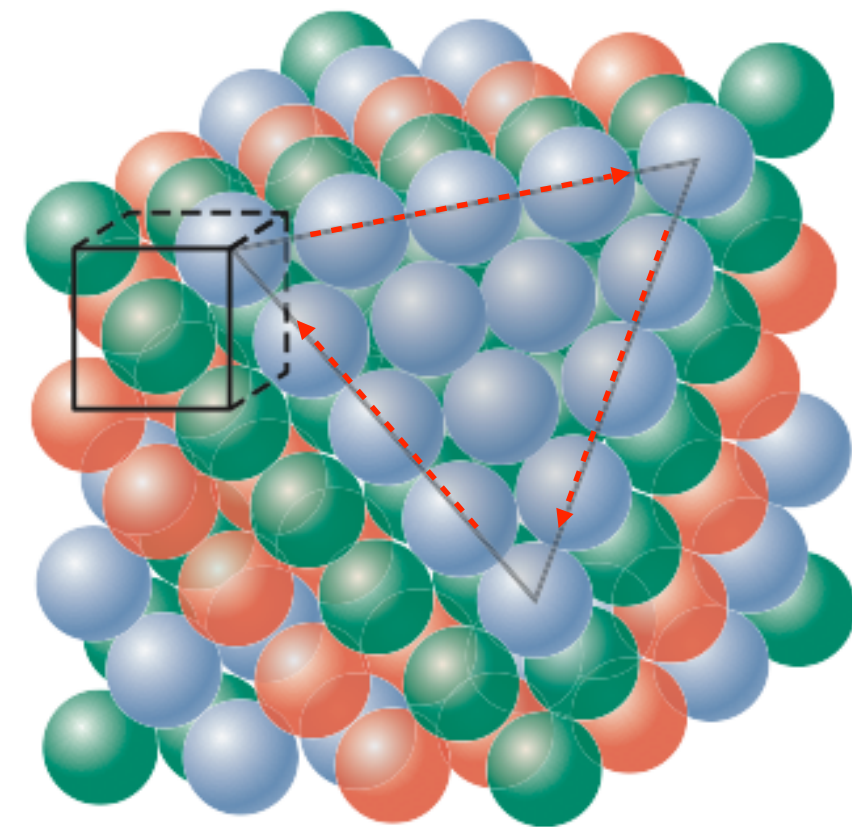
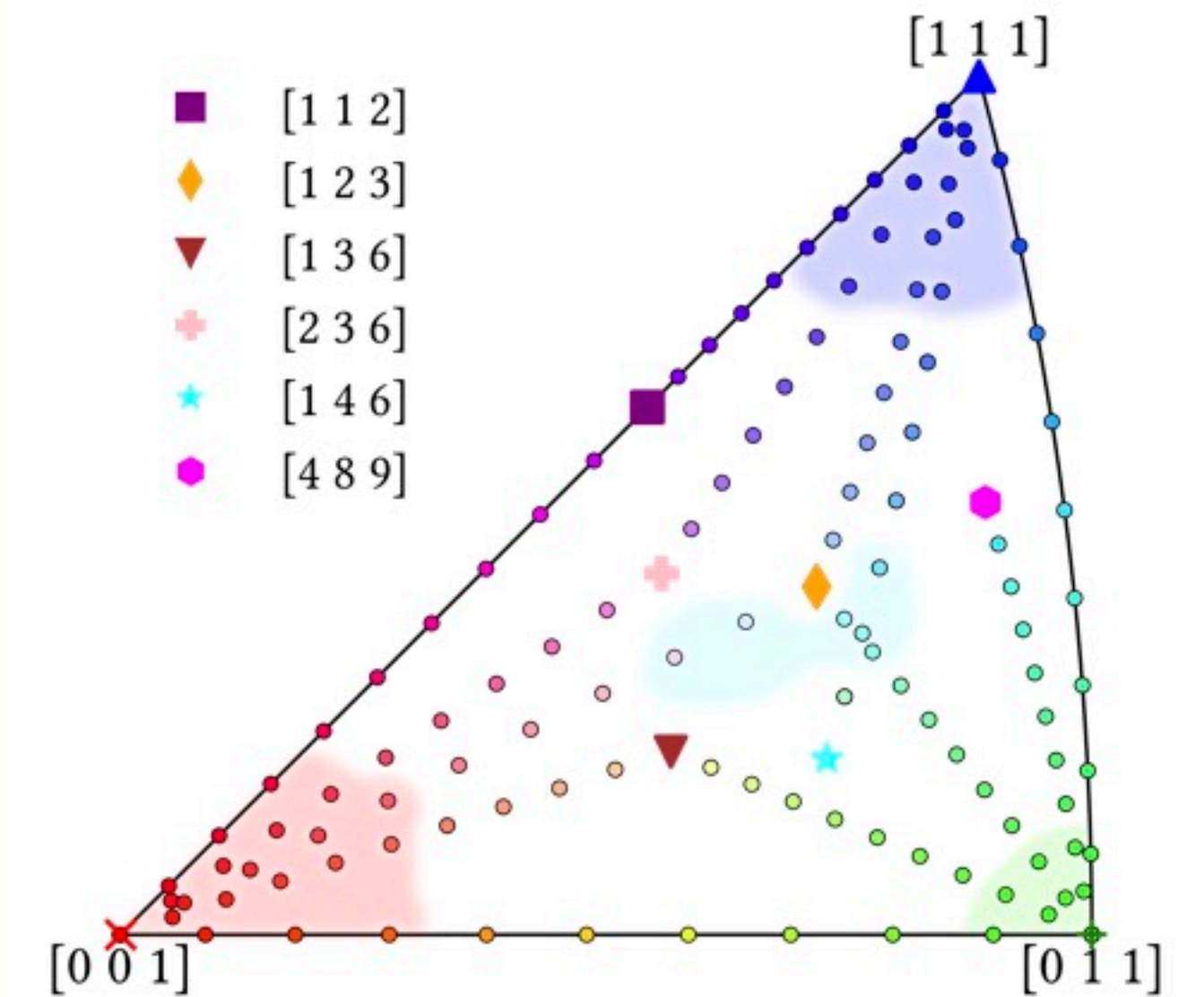
Dislocation link lengths are exponentially distributed

Dislocation link lengths are analyzed across different loadings

Loading orientation near [001]



Q2: ... link length distribution under general loading orientations?



FCC (Cu) has 12 slip systems.

Q1: What about link length distribution on individual slip systems?

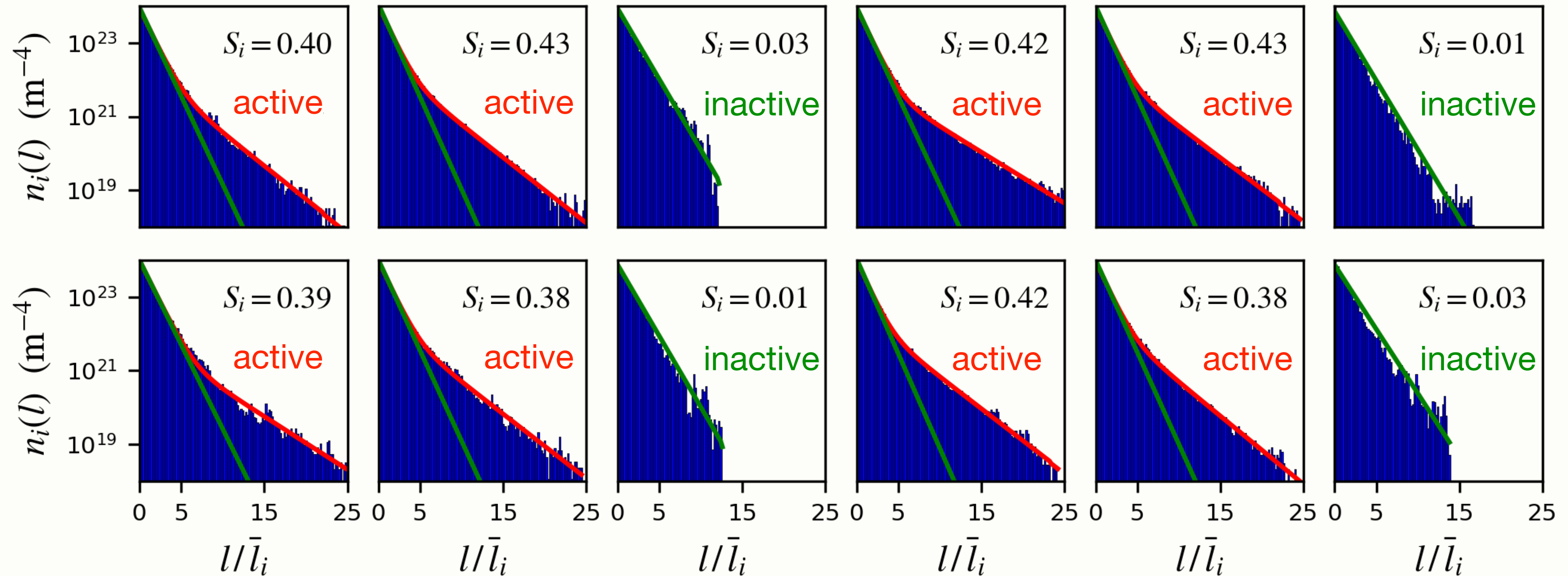
Link statistics were analyzed over 118 loading orientations, on individual slip systems.

Key features of link distributions

*Different distributions on
active & inactive slip systems*

Link statistics near [001]: double exponential for active slip systems

Loading orientation: [0.03, 0.05, 0.99]

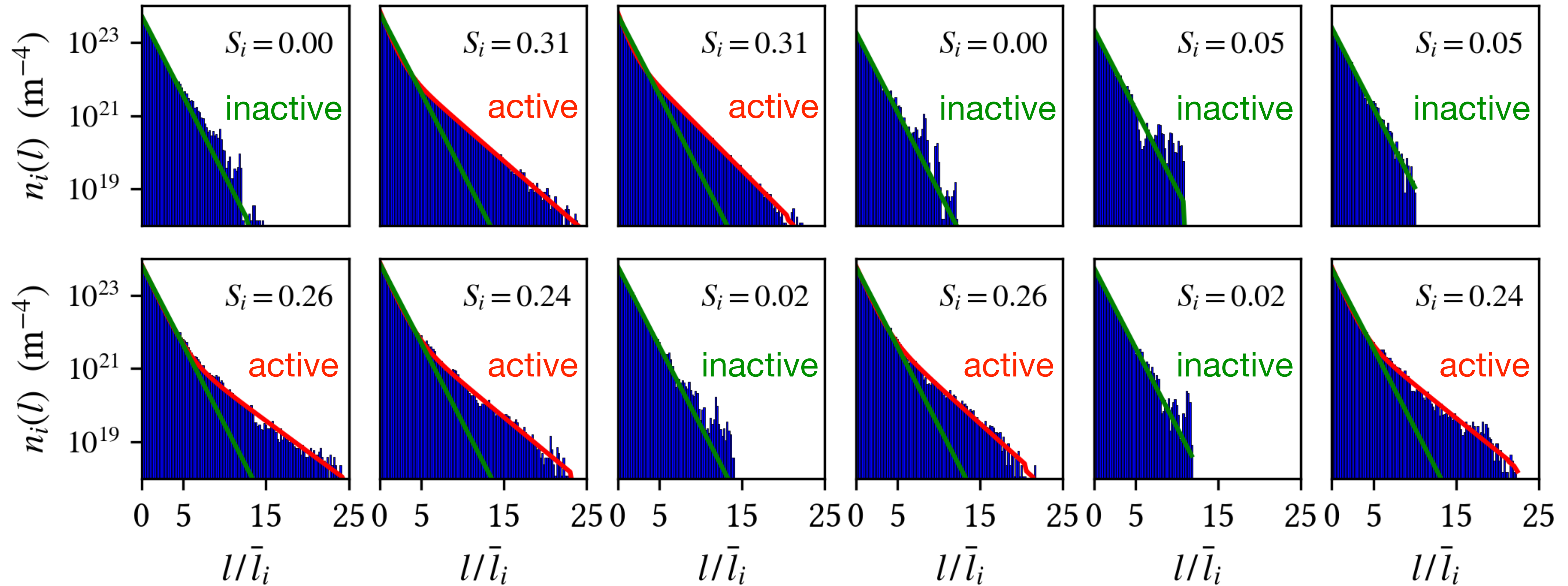


Single exponential: $n_i(l) = \frac{N_i}{\bar{l}_i} e^{-l/\bar{l}_i}$

Double exponential: $n_i(l) = \frac{N_i^{(1)}}{\bar{l}_i^{(1)}} e^{-l/\bar{l}_i^{(1)}} + \frac{N_i^{(2)}}{\bar{l}_i^{(2)}} e^{-l/\bar{l}_i^{(2)}}$

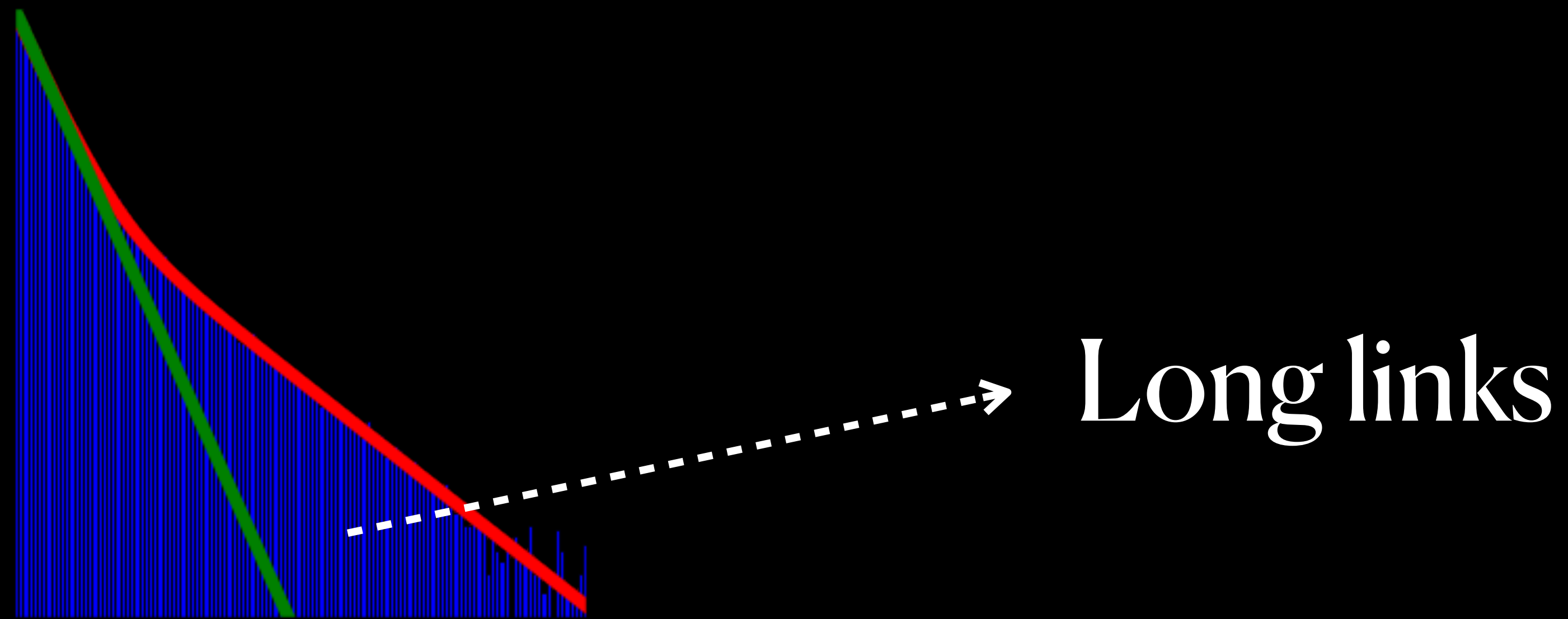
Link statistics near [111]: double exponential for active slip systems

Loading orientation: [0.53, 0.60, 0.60]



Single exponential: $n_i(l) = \frac{N_i}{\bar{l}_i} e^{-l/\bar{l}_i}$

Double exponential: $n_i(l) = \frac{N_i^{(1)}}{\bar{l}_i^{(1)}} e^{-l/\bar{l}_i^{(1)}} + \frac{N_i^{(2)}}{\bar{l}_i^{(2)}} e^{-l/\bar{l}_i^{(2)}}$

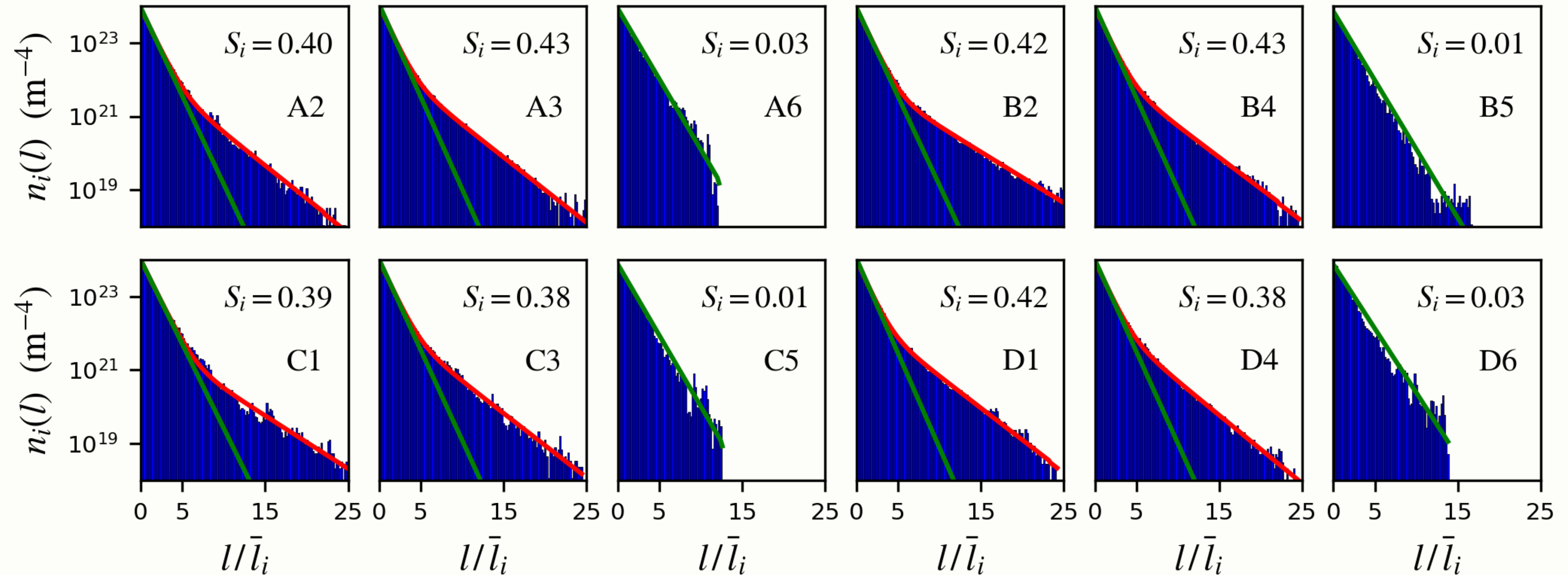


What caused longer links?

Hypothesis: *applied stress* \rightarrow *plastic flow*

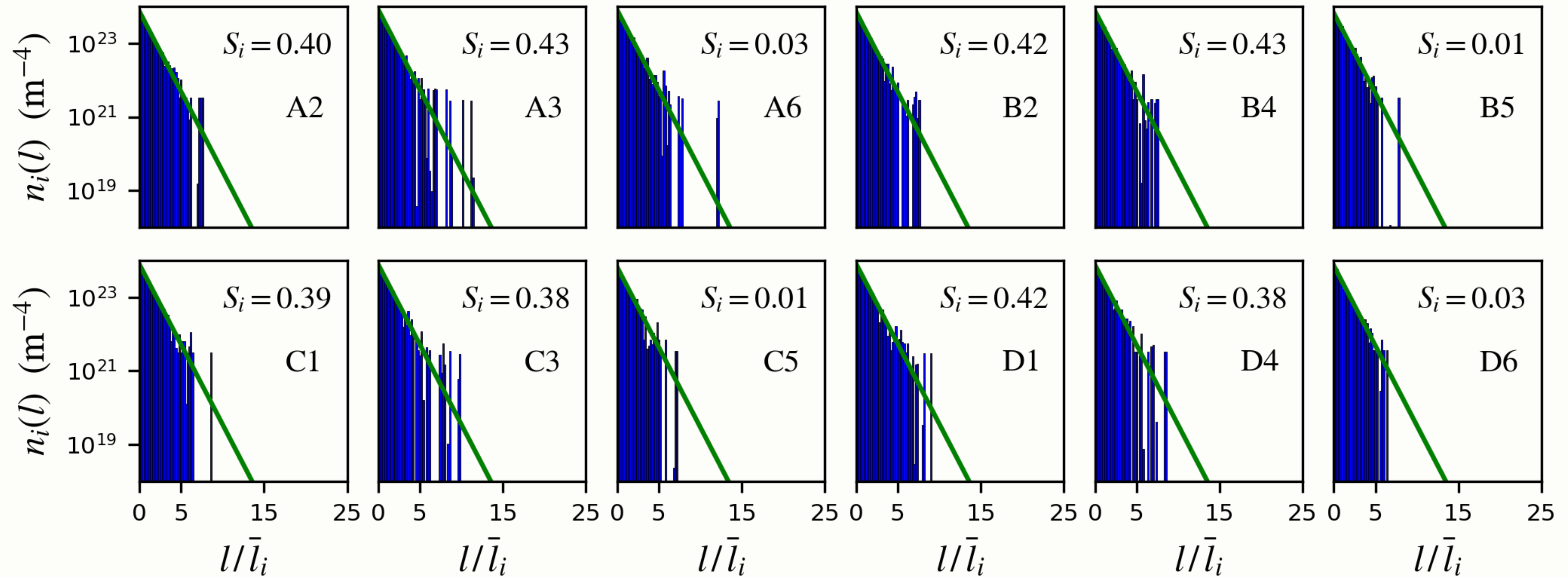
Link statistics near [001]: double exponential for active slip systems

Loading orientation: [0.03, 0.05, 0.99]



Testing the hypothesis: **remove applied stress!**

Link statistics near [001]: relaxed to a single exponential distribution

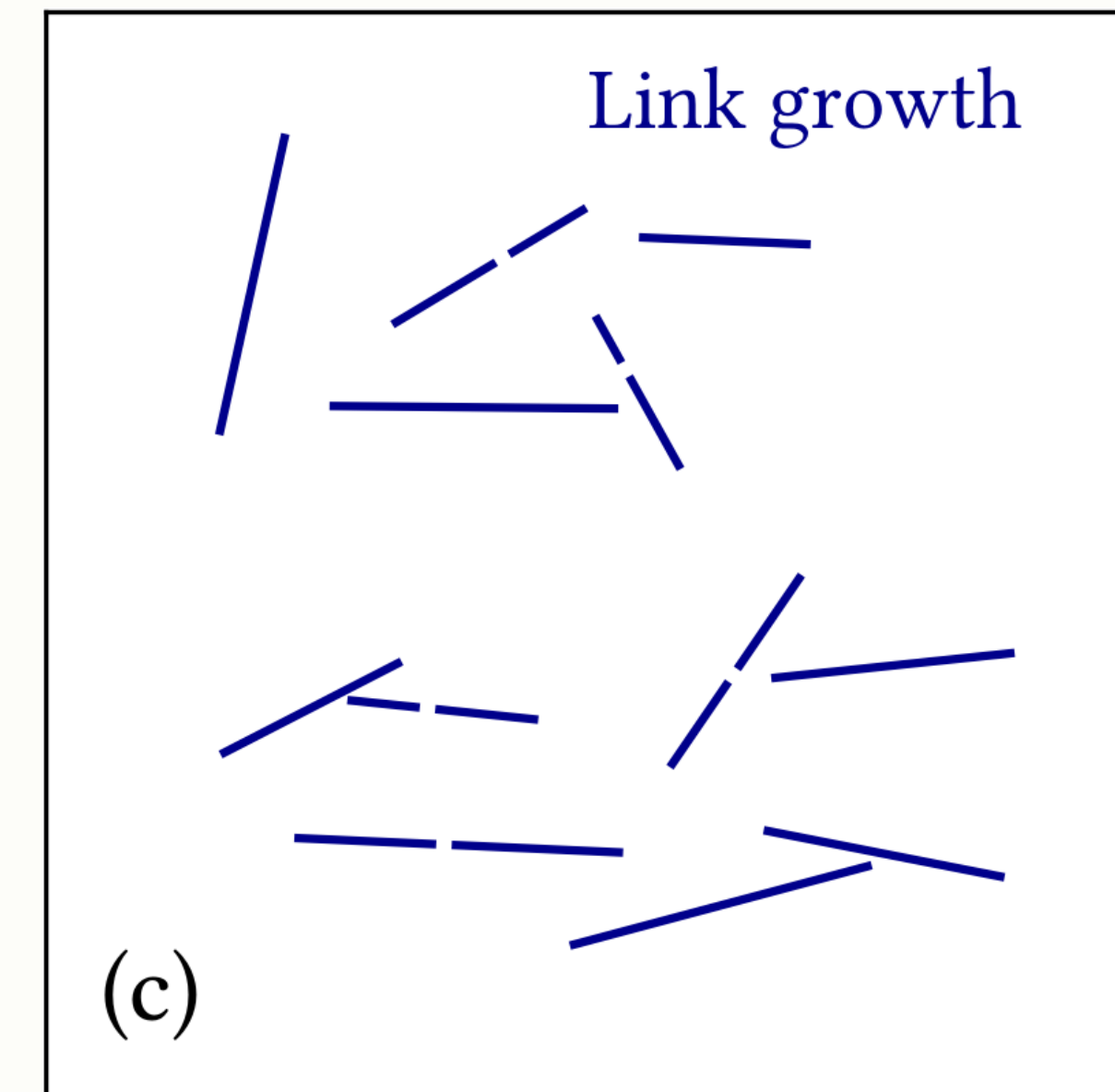
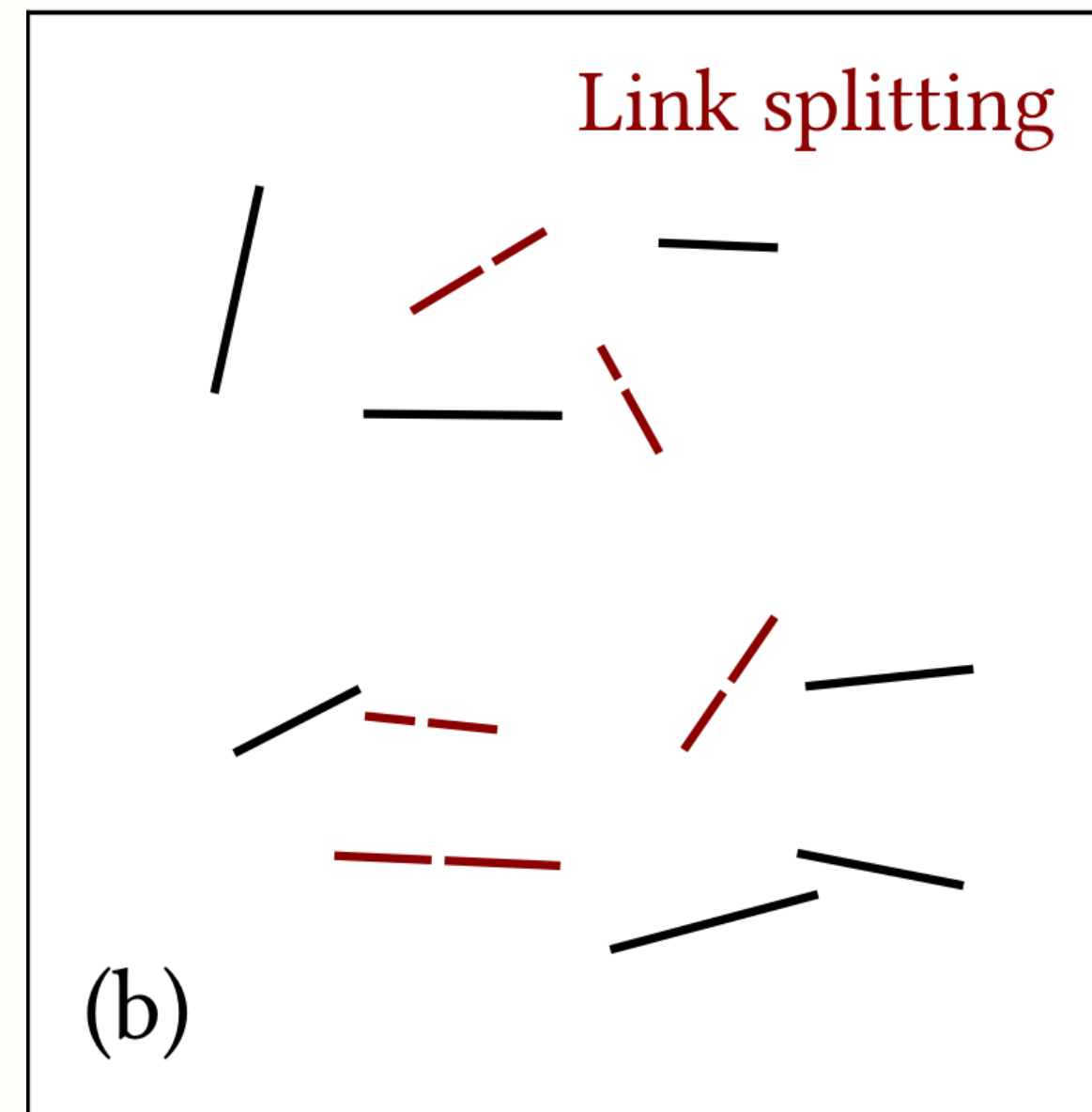
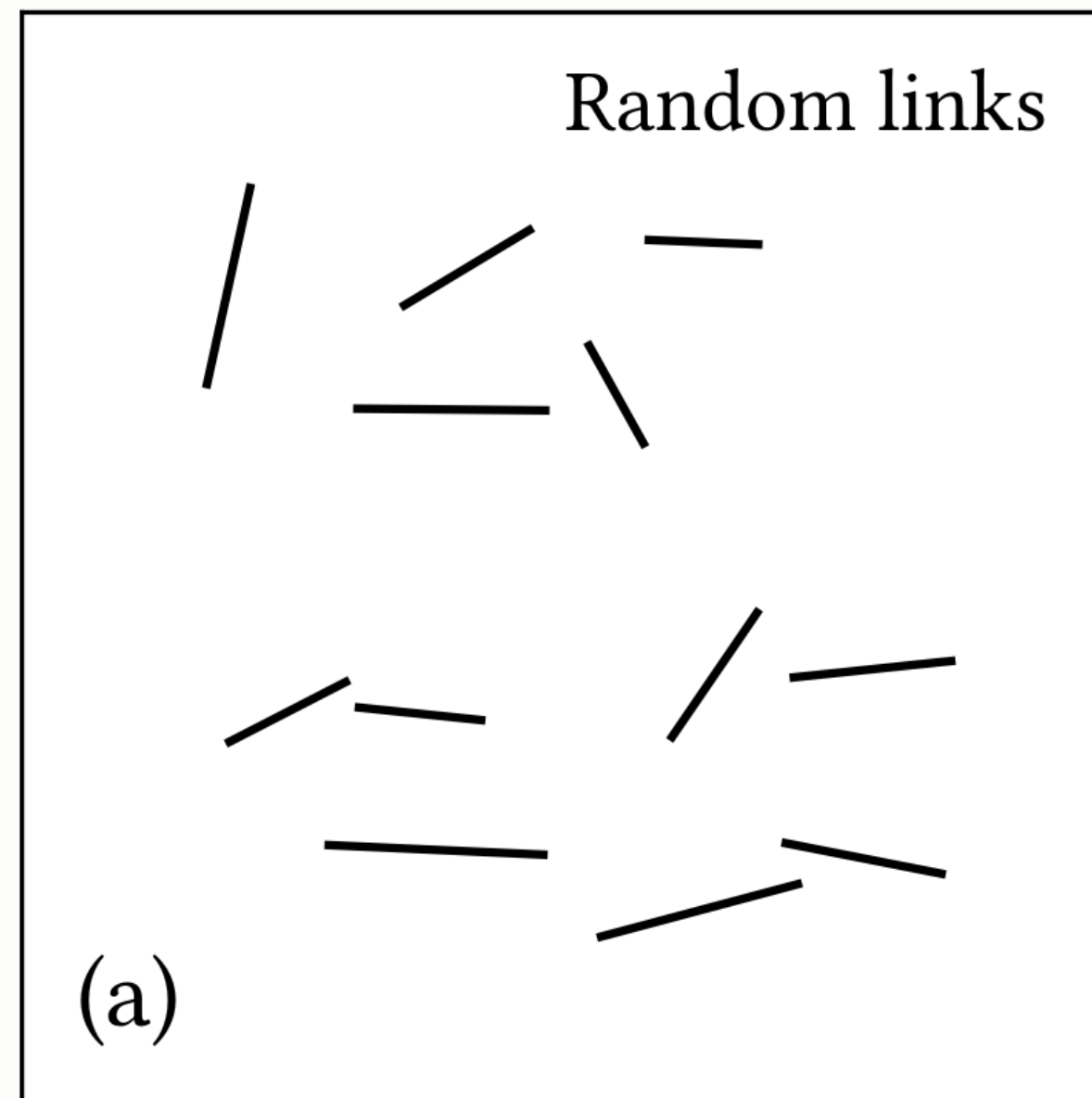


Loading orientation: [0.03, 0.05, 0.99] (relaxed at 0.9% $\dot{\gamma}_d$)

Why double exponential?

Generalized Poisson process models explains link distributions

A mathematical model inspired by dislocation behavior during plastic deformation



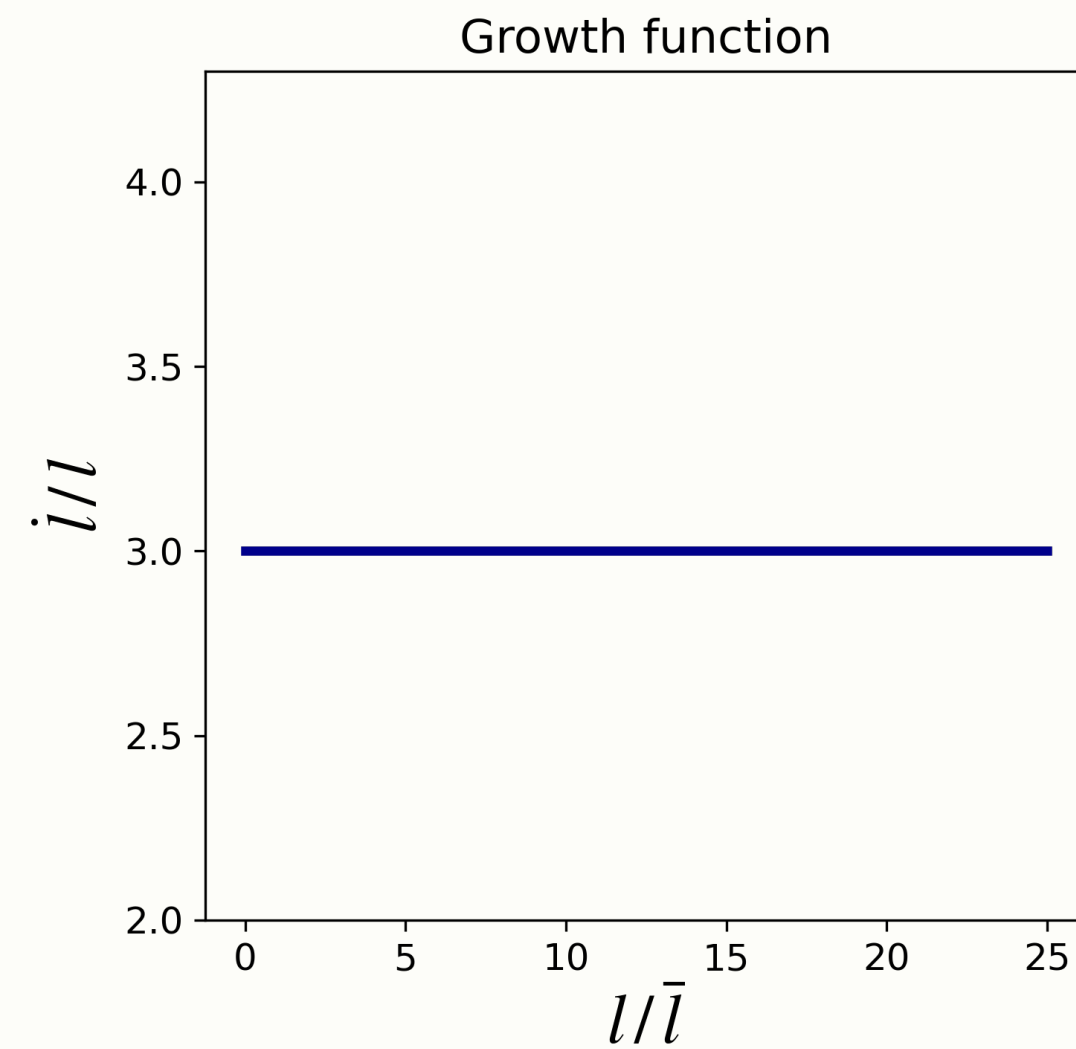
Split probability rate is proportional
to the link length:

$$r_k = A \cdot \frac{l_k}{\bar{l}}$$

Link growth follows a growth function
(of the normalized link length):

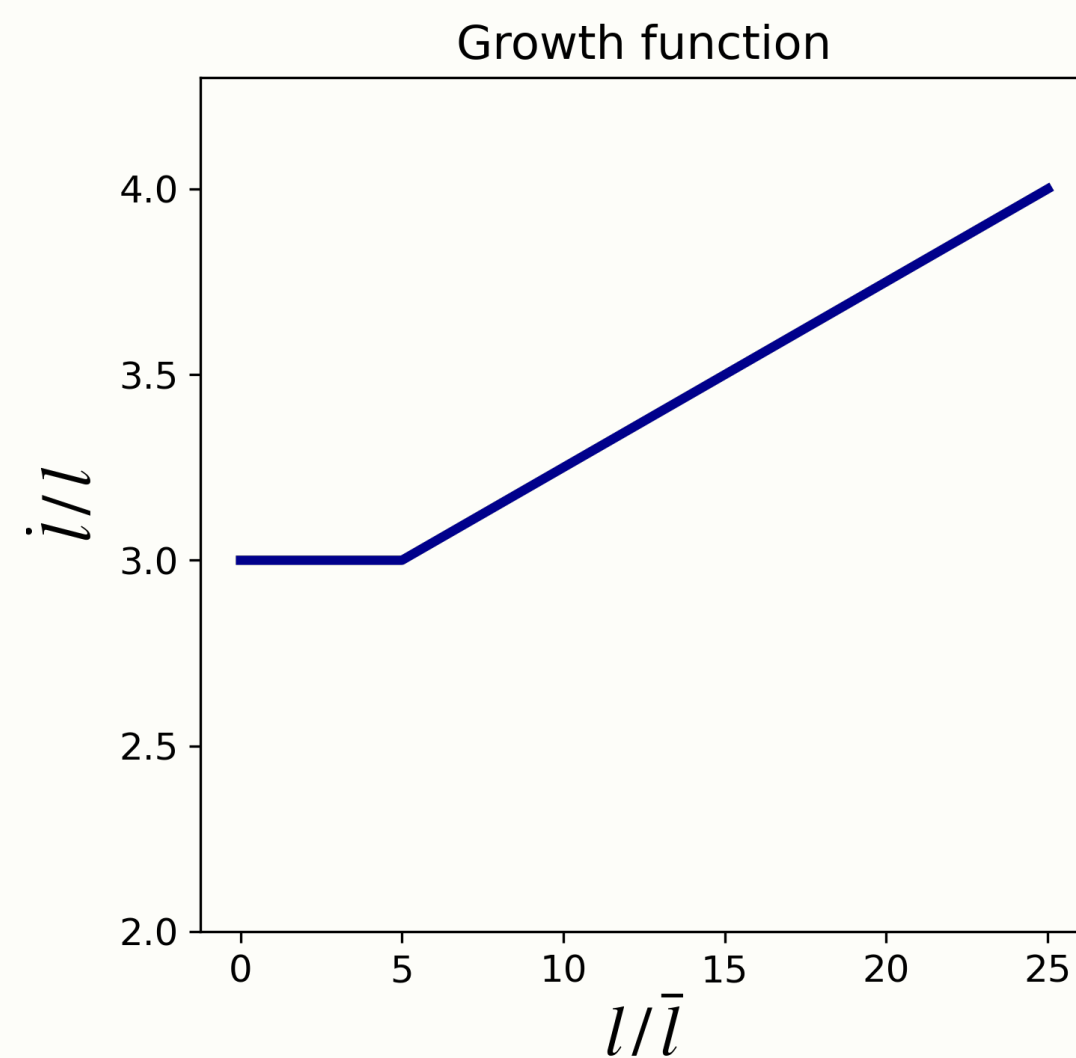
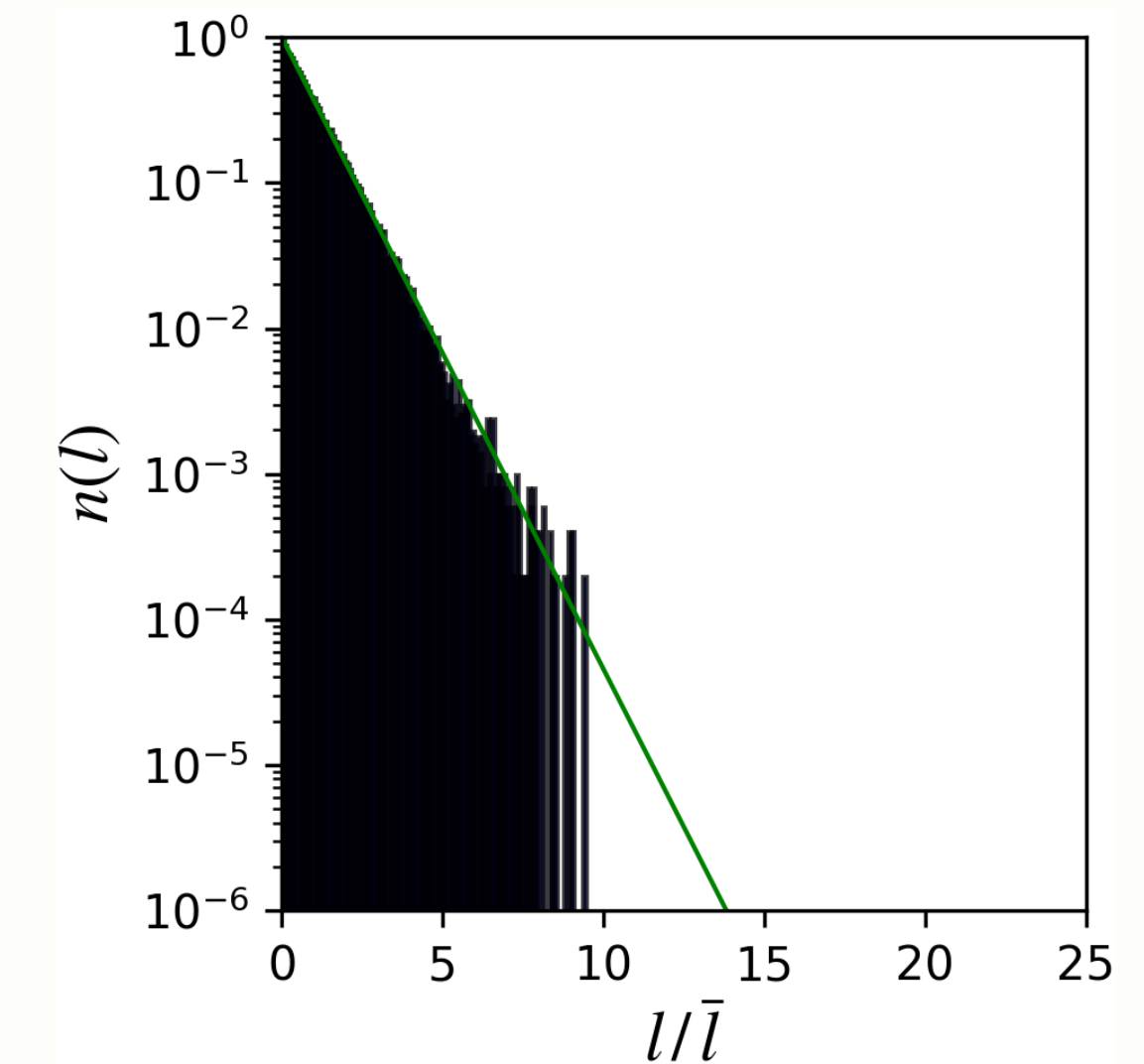
$$\dot{l}_k / l_k = G(l_k / \bar{l})$$

Generalized Poisson process models explains link distributions



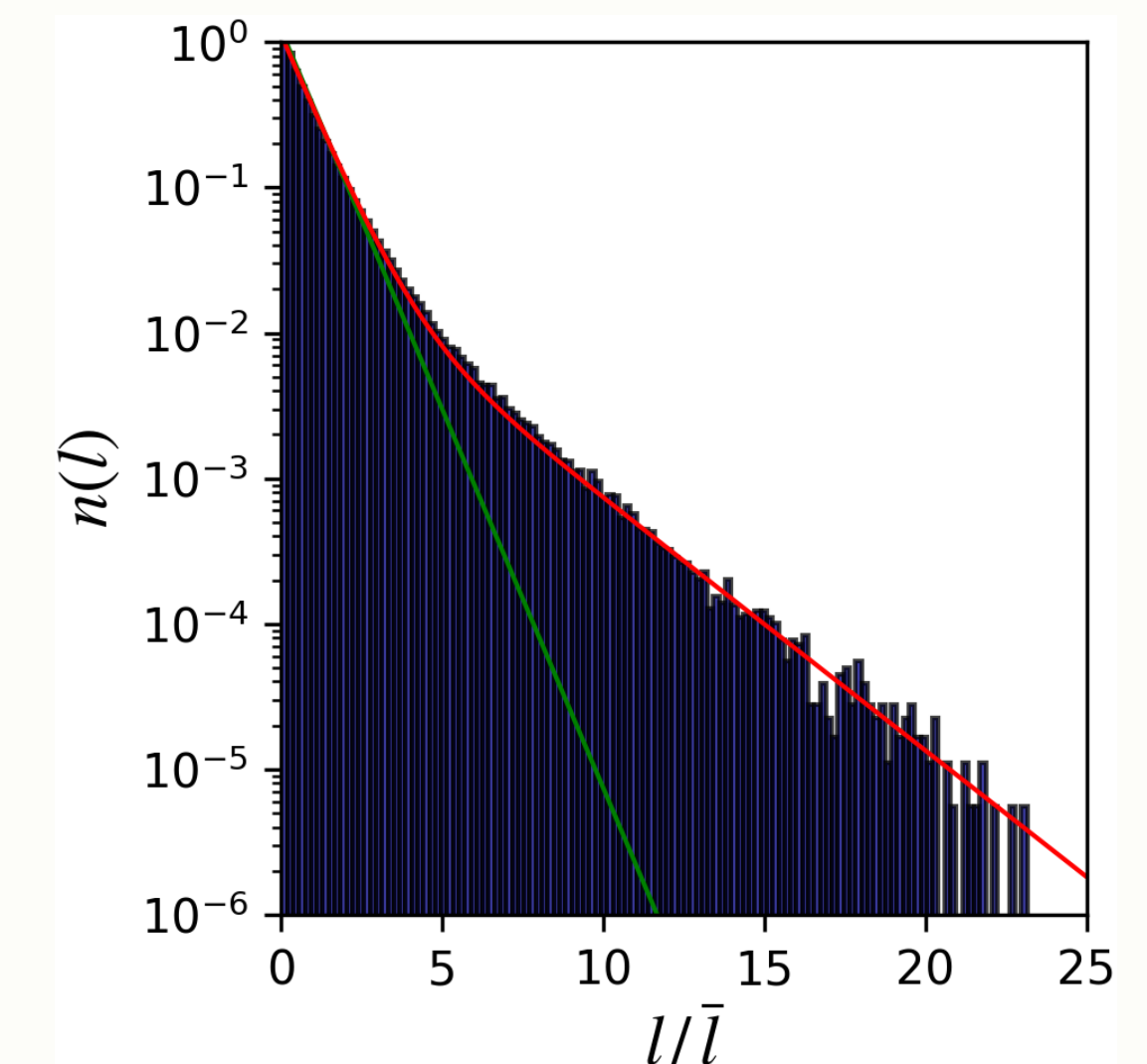
Constant growth of i/l leads to single exponential distribution.

(Equivalent with no growth)



Piecewise linear growth of i/l leads to double exponential distribution.

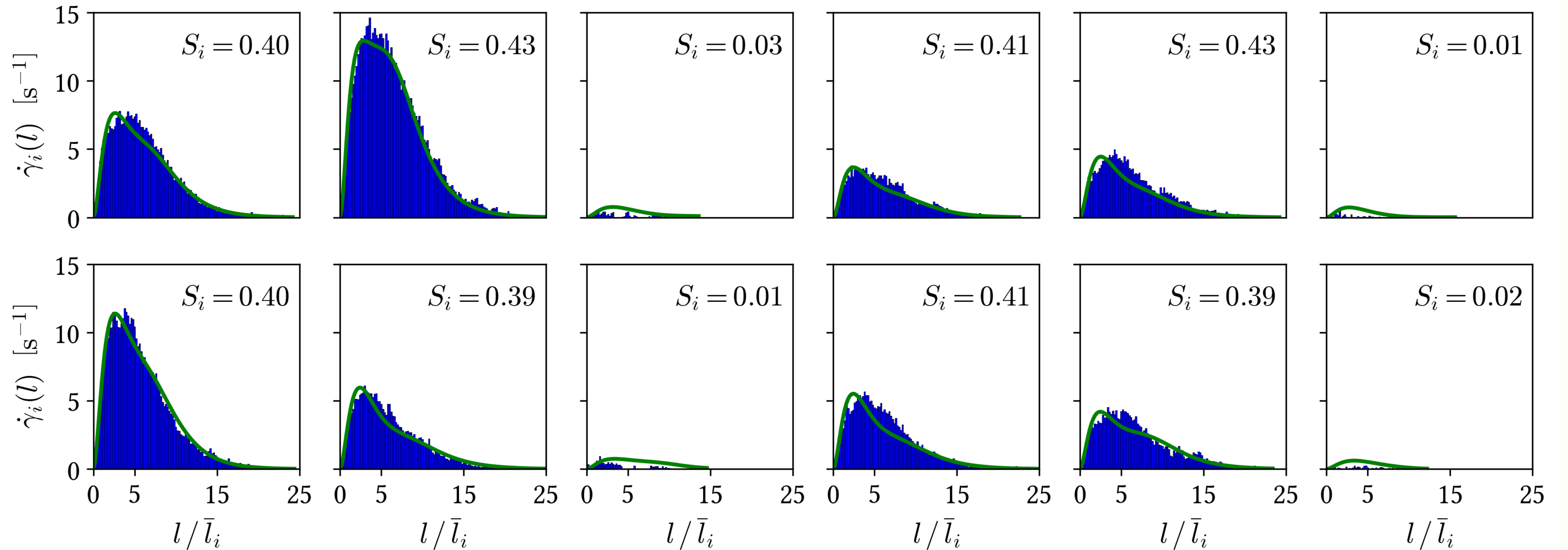
(Or other functions that conform to a similar qualitative form)



Crystal plasticity: *link length* \rightarrow *shear rates*

Shear rates distributions as a function of link length

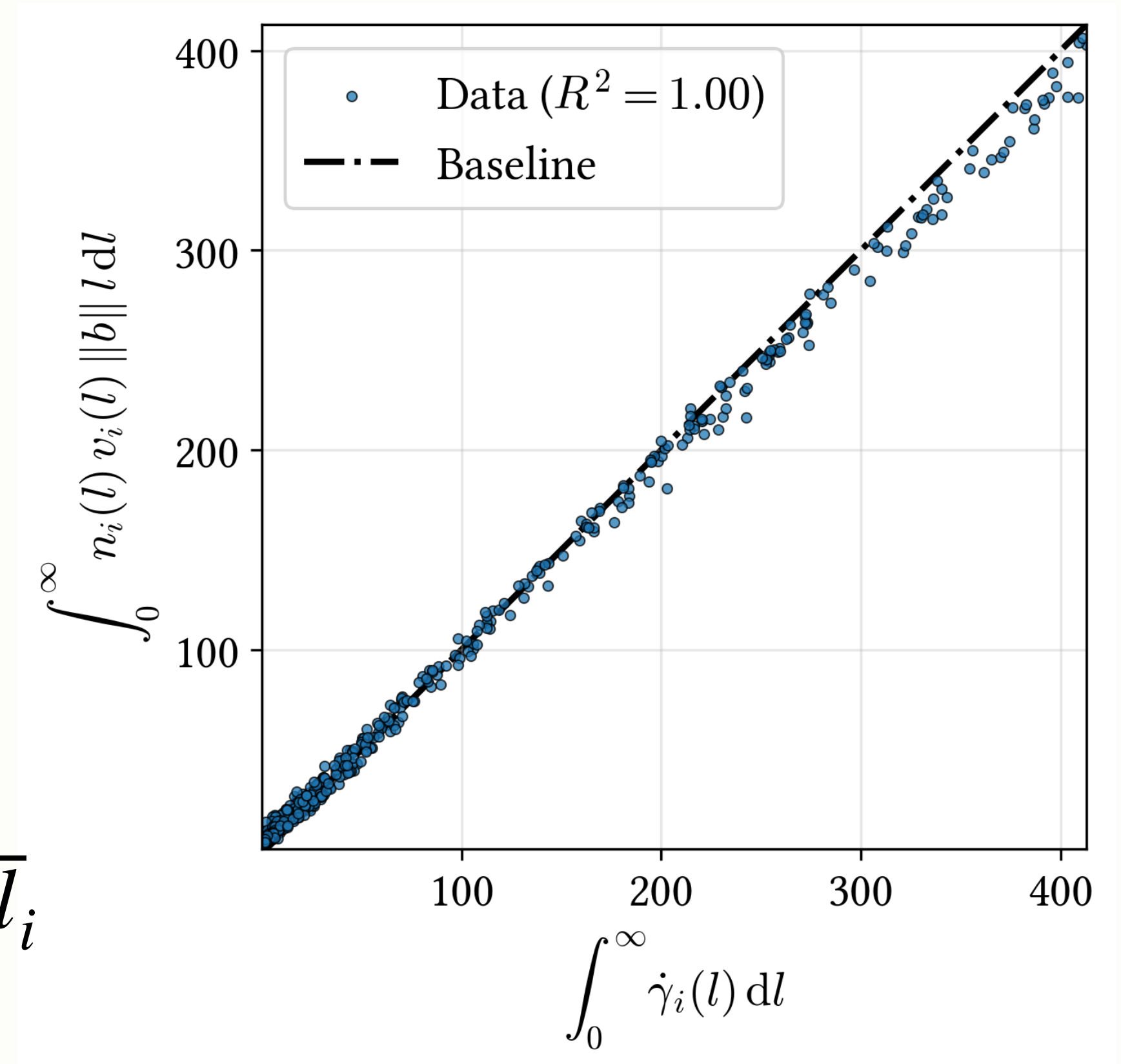
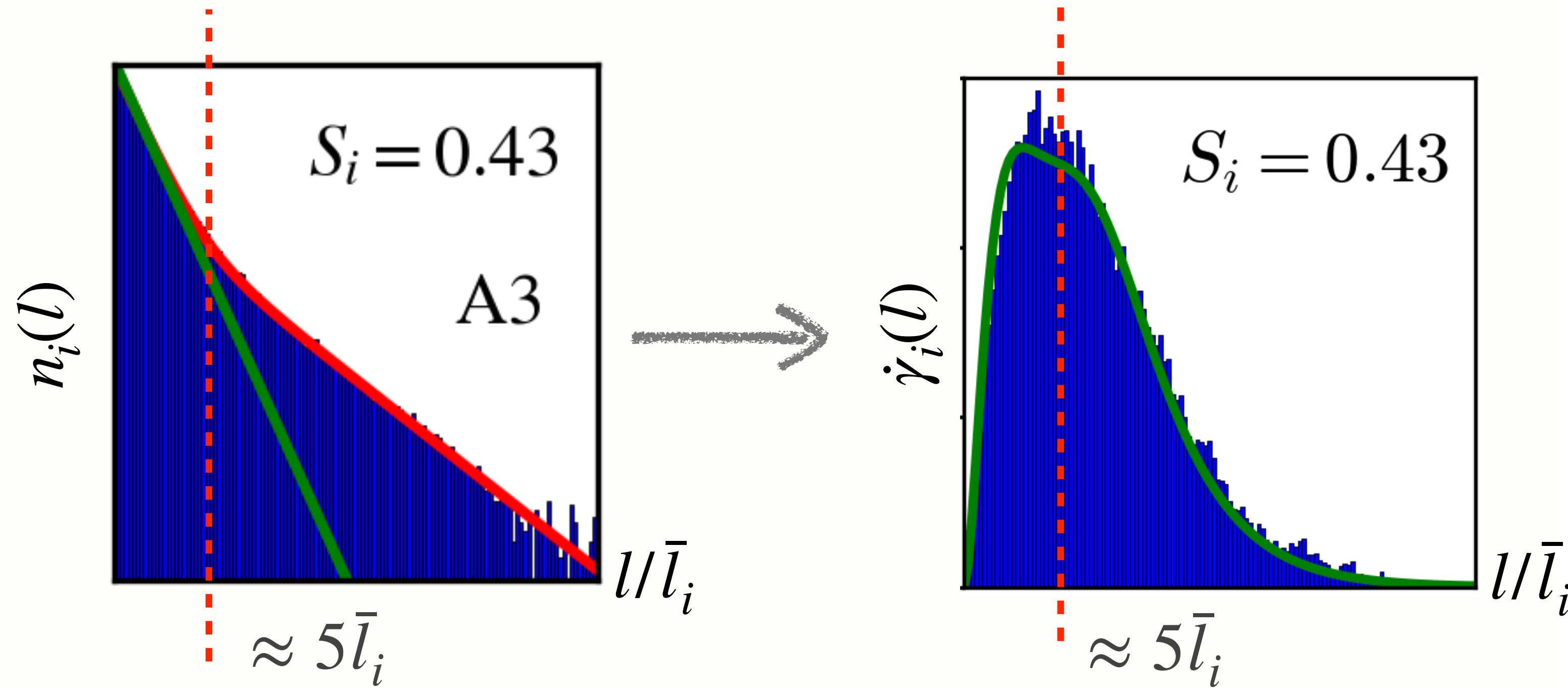
Loading orientation: [0.01, 0.04, 0.99]



We postulate velocity function-based flow rule — can predict shear rates (as a function of link length) accurately on individual slip systems across different loading orientations.

Shear rates distributions can be accurately predicted

Loading orientation near [001]



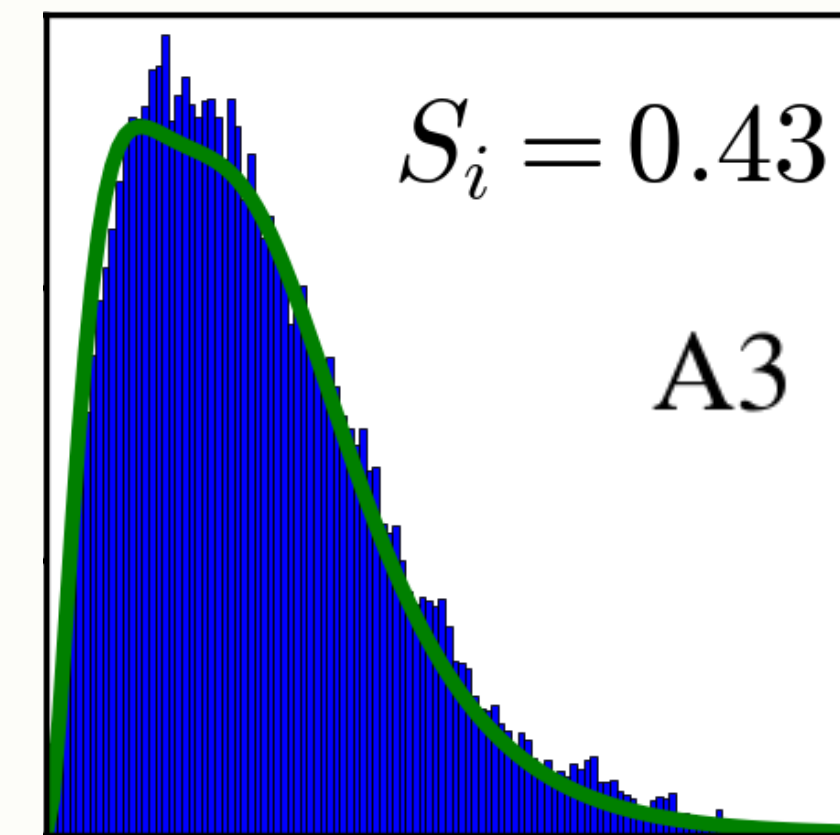
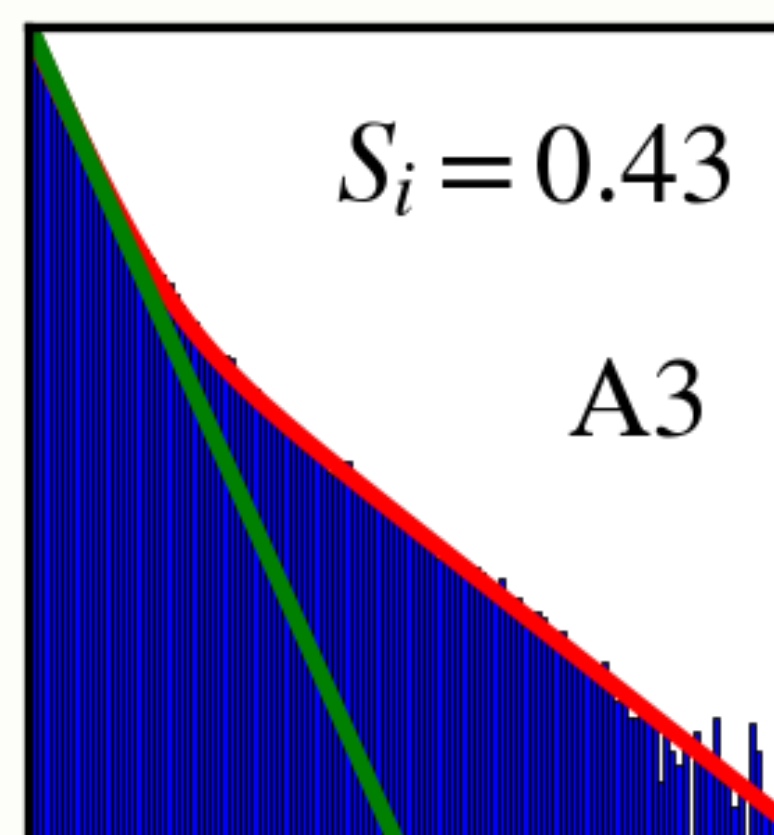
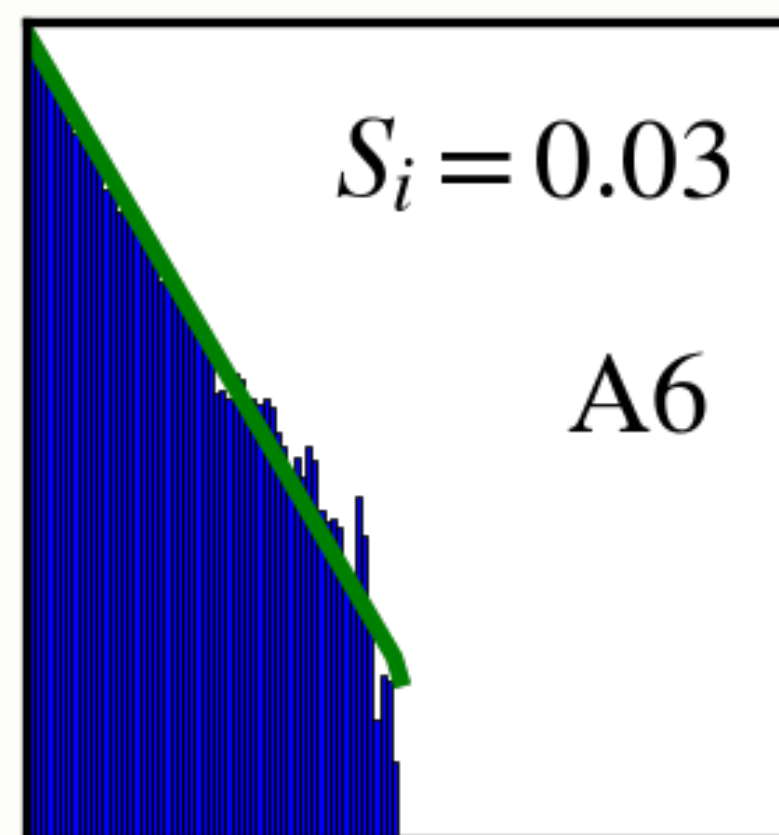
Shear rate (on individual slip system) as a function of link length peaks at around $l \approx 5\bar{l}_i$.

Longer links ($\geq 5\bar{l}_i$) contribute significantly to the shear rates (as a function of l).

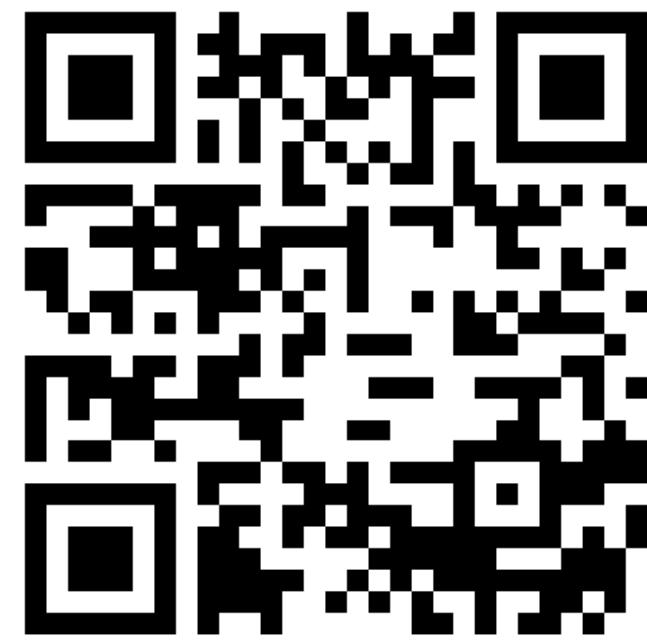
Overall shear strain rates can be predicted accurately.

Summary

- ▶ Inactive slip systems follow a **single-exponential distribution**.
- ▶ Active slip systems follow a **double-exponential distribution** with a long tail.
- ▶ A **generalized Poisson process** with growth rules explains both single- & double-exponentials.
- ▶ Longer links **contribute significantly** to shear rates; one can **predict strain rates** from link statistics.



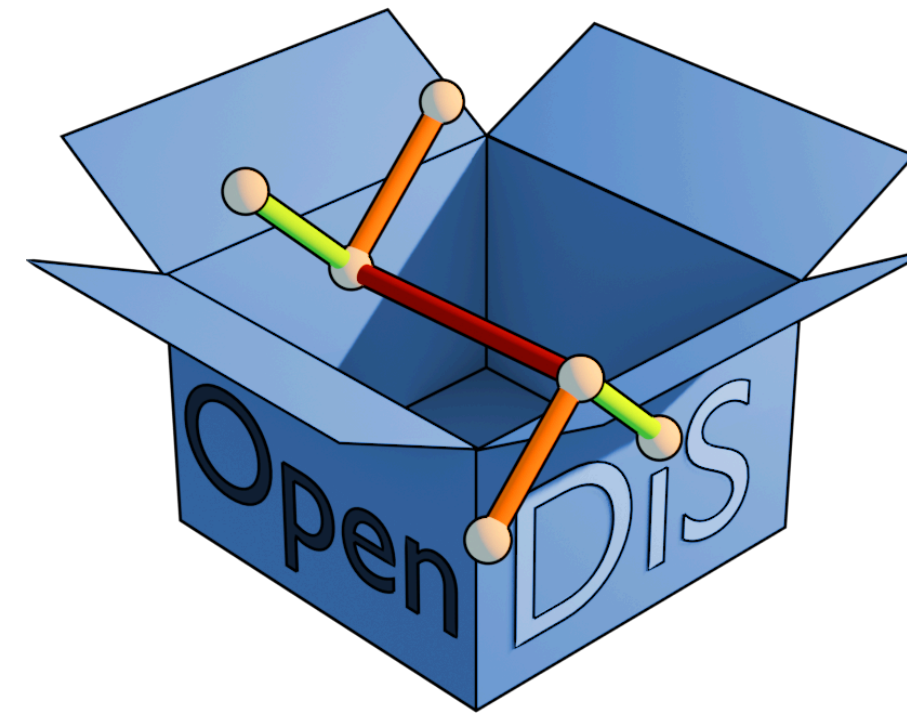
Q & A



Paper

J. Mech. Phys. Solids, 210, 106533 (2026).

DOI: [10.1016/j.jmps.2026.106533](https://doi.org/10.1016/j.jmps.2026.106533)



OpenDiS

Open source DDD code. (Python & C++)

<https://github.com/OpenDiS/OpenDiS>

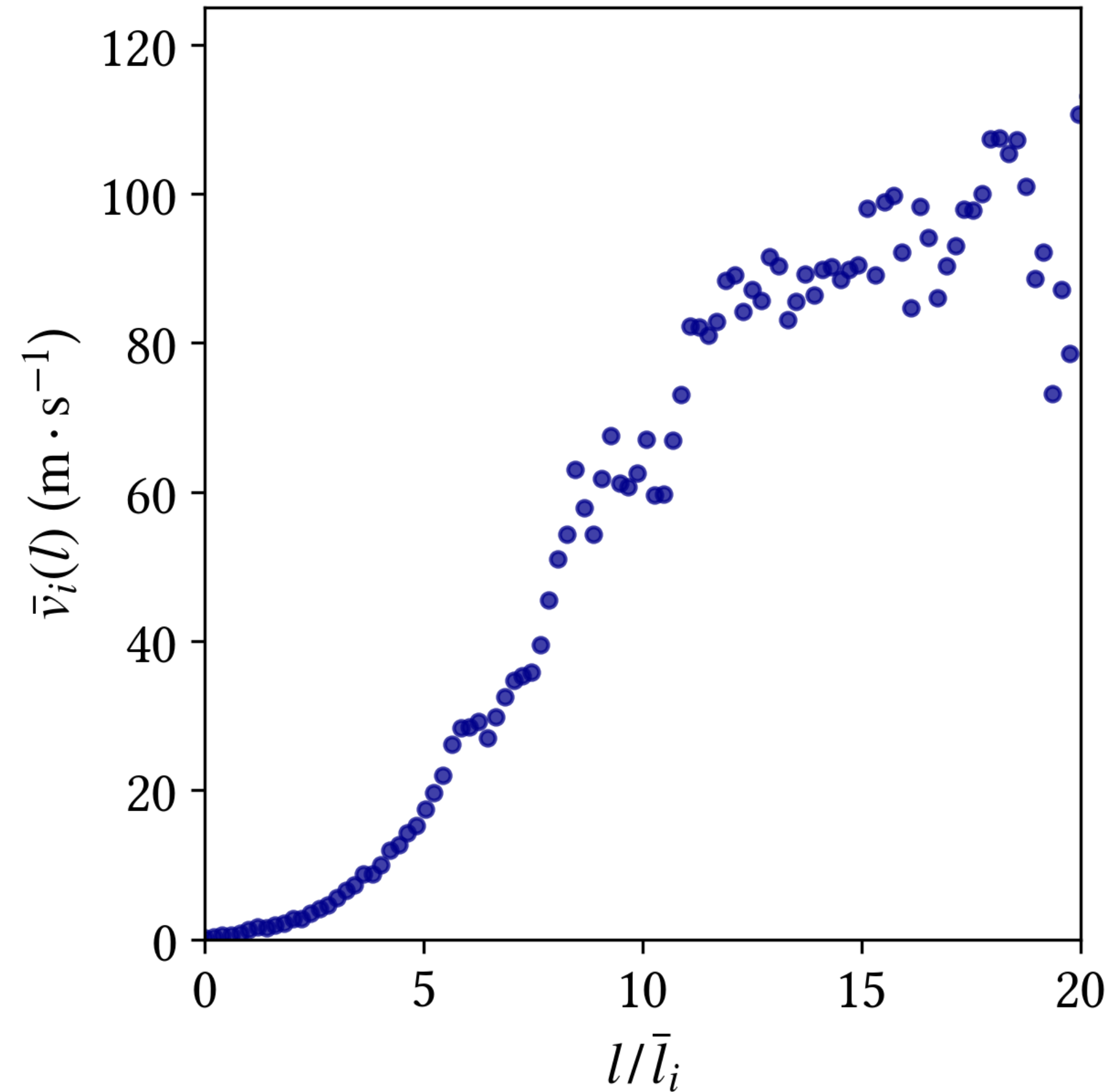
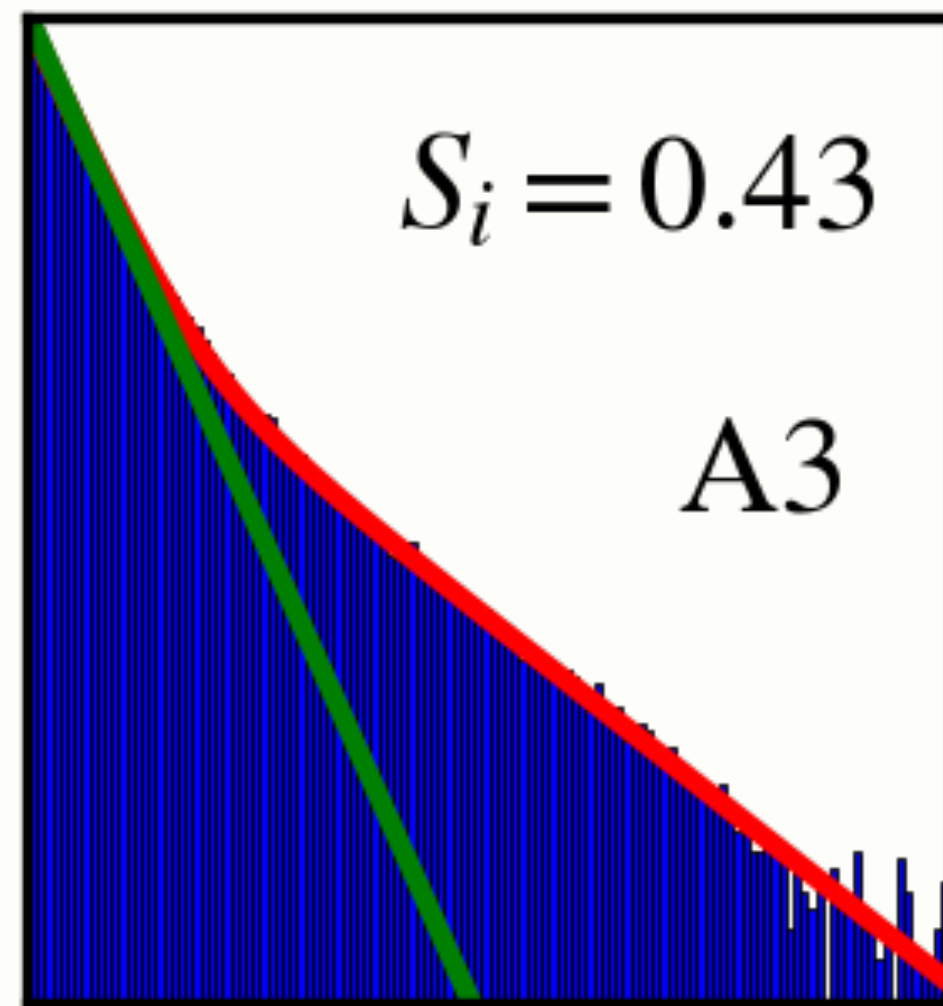
Contact: hzhai@stanford.edu (H.Z.); caiwei@stanford.edu (W.C.)

Supplementary Slides

Mobility of dislocation links

Link velocity is defined as shear rates divided by link length distributions times link length:

$$\bar{v}_i(l) = \dot{\gamma}_i(l) / (l b n_i(l))$$

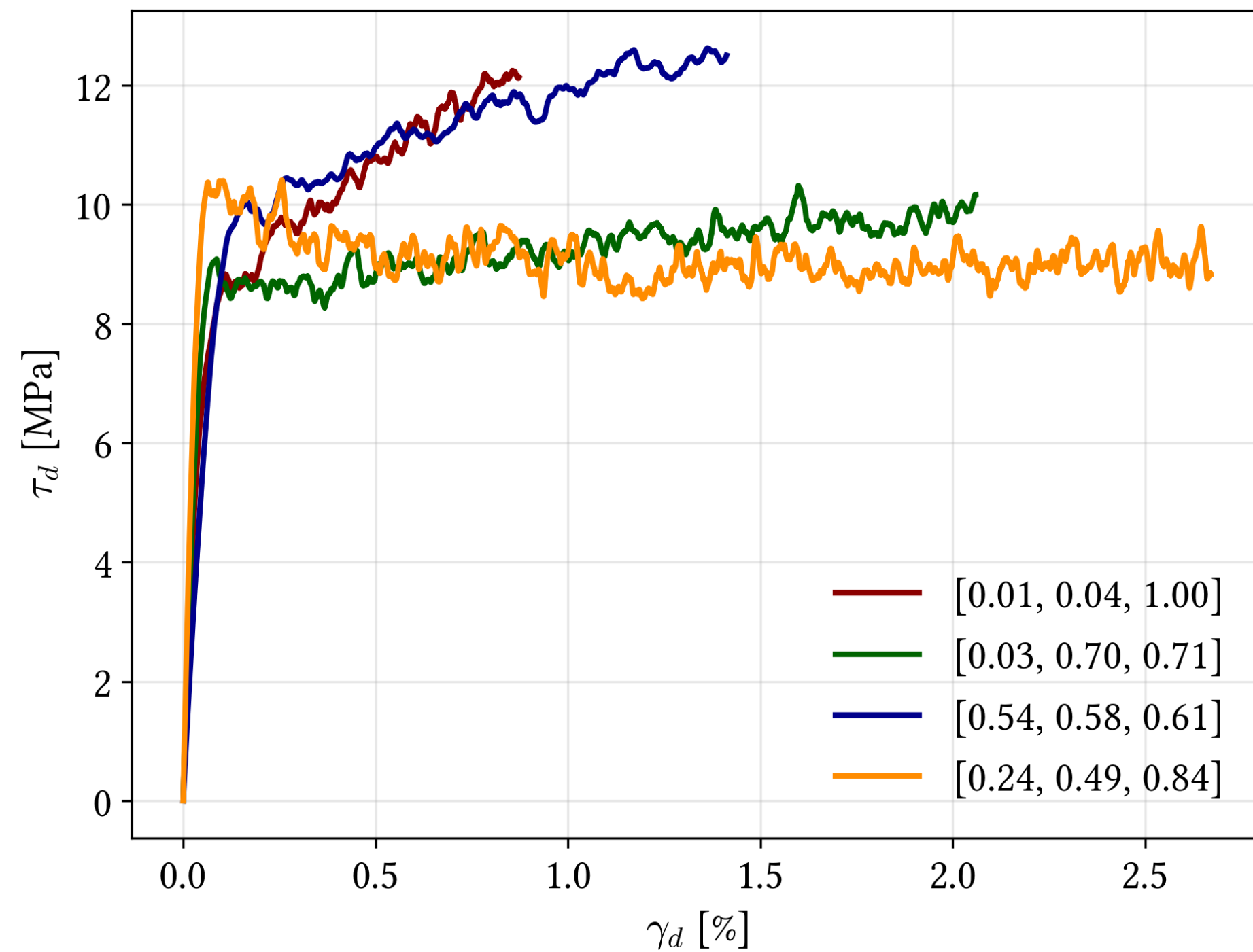


Longer links are highly mobile (higher velocity) during strain hardening.

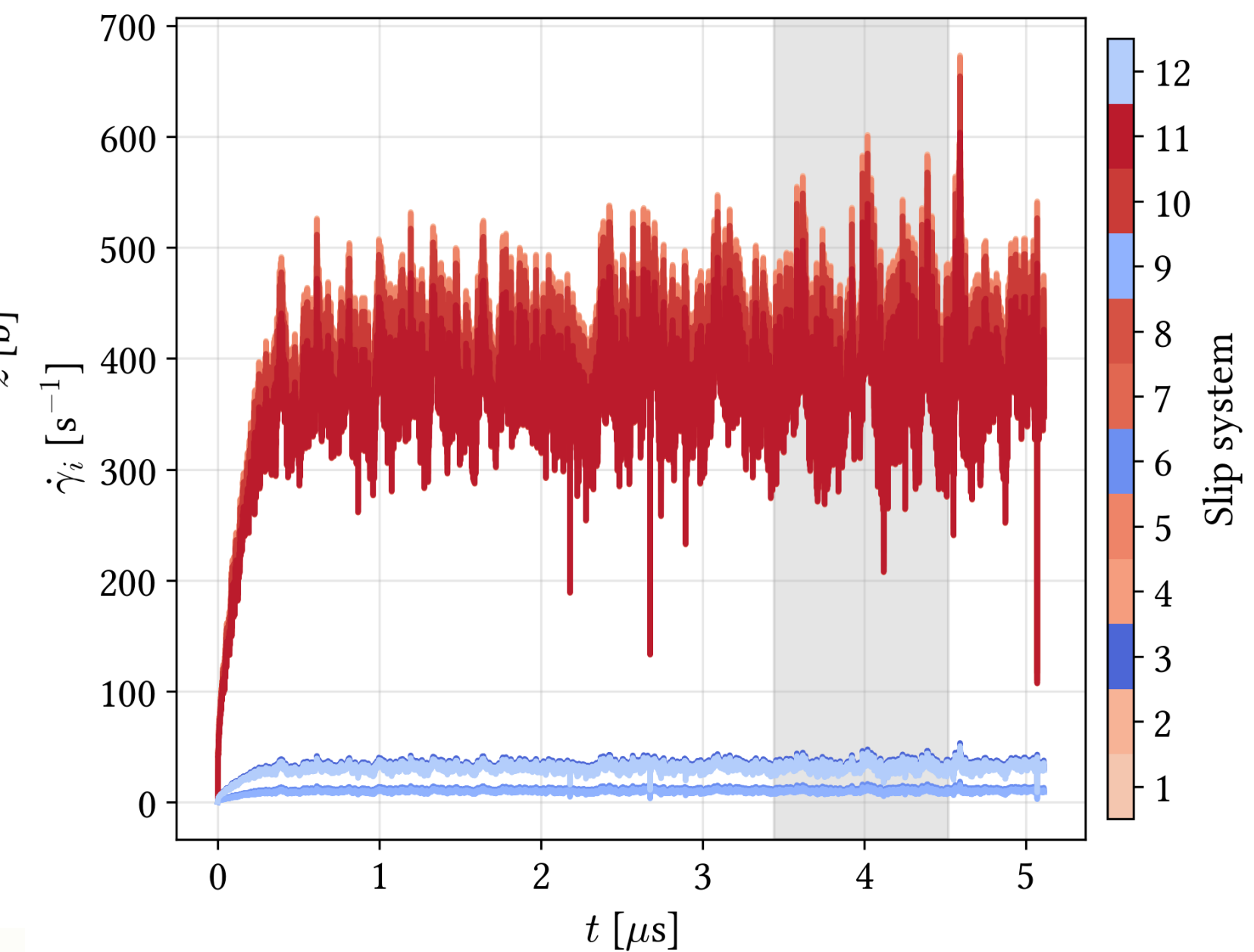
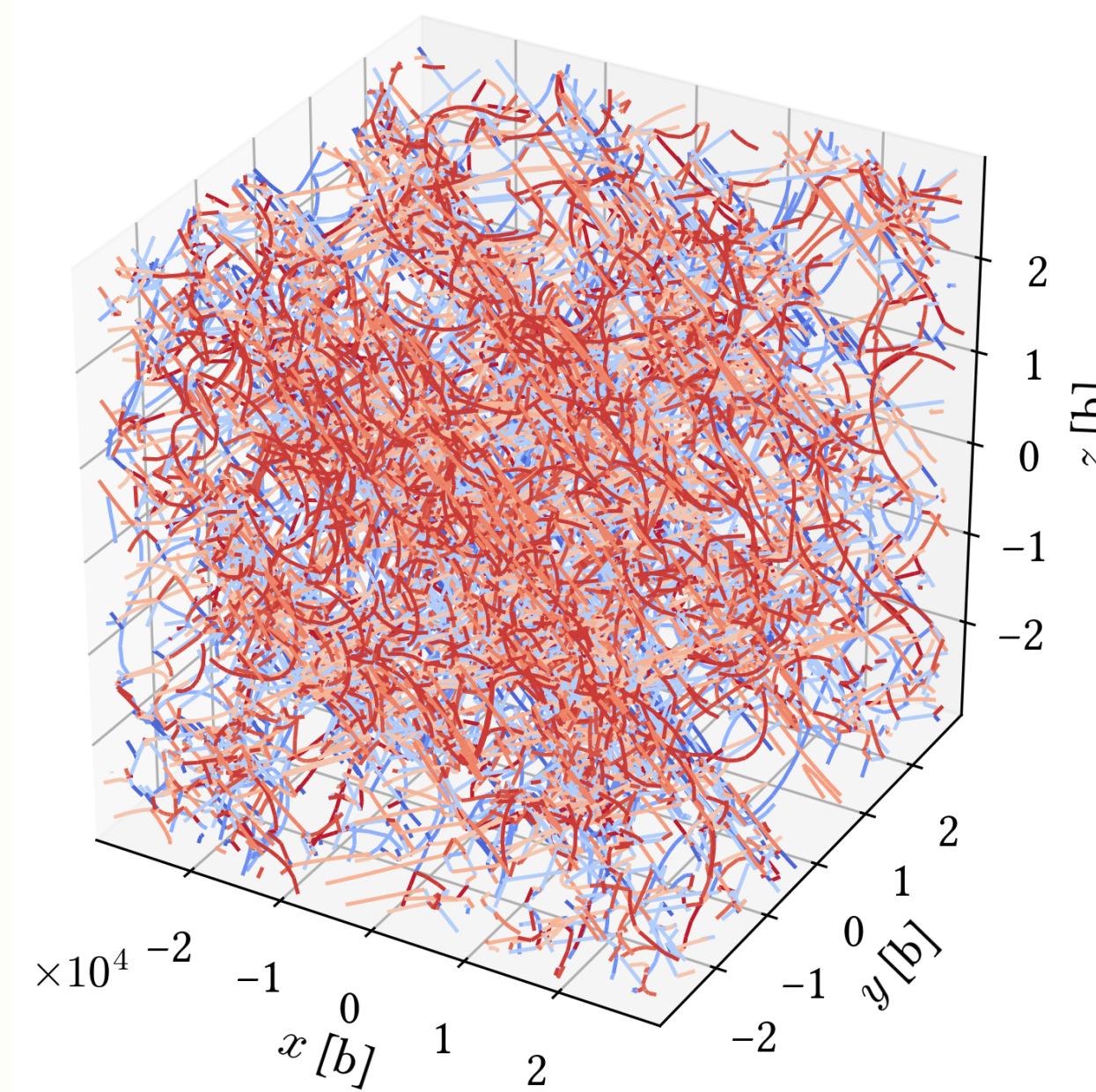
From link statistics to flow rule

Q: Can you predict strain rates from link length statistics (on individual slip systems)?

Link length distribution $n_i(l)$ relates to shear rates $\dot{\gamma}_i$ via dislocation line motion, i.e., the velocity v_i .



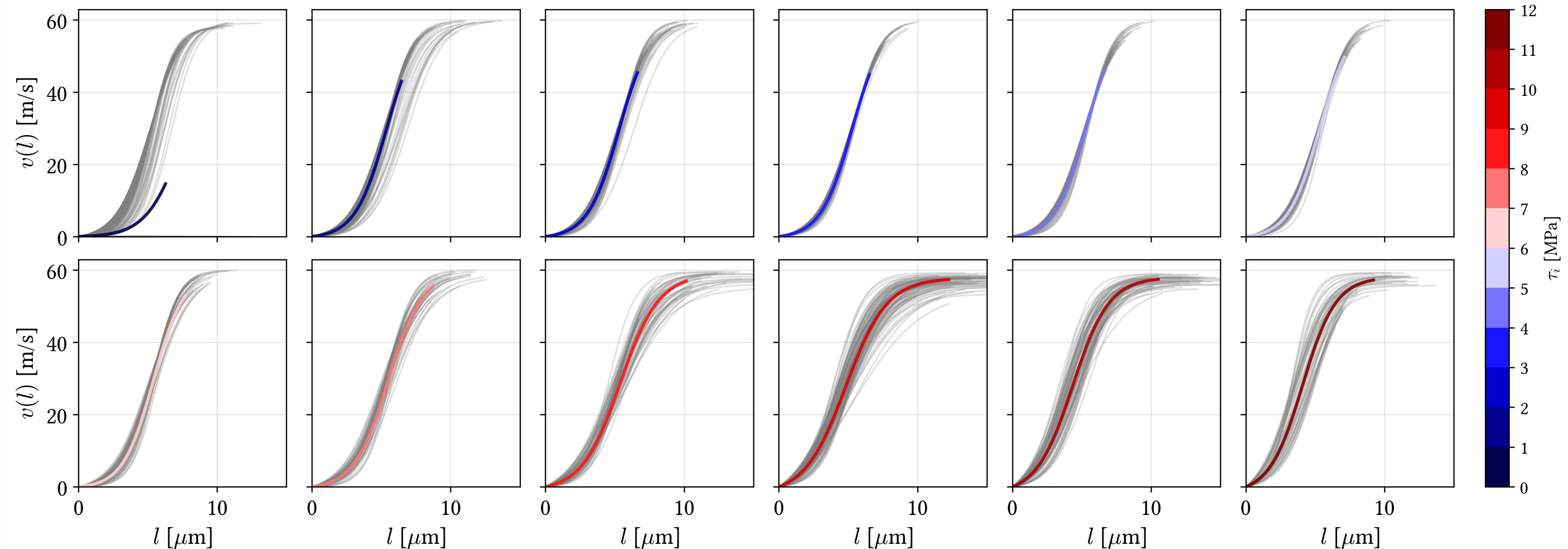
Stress-strain curves behave differently (different hardening rates) under different loading orientations.



Loading orientation: [0.01, 0.04, 0.99]

Flow rule from link statistics

We hypothesize there exists a velocity function $v_i(l)$ that can describe the motion of dislocation lines during strain hardening.



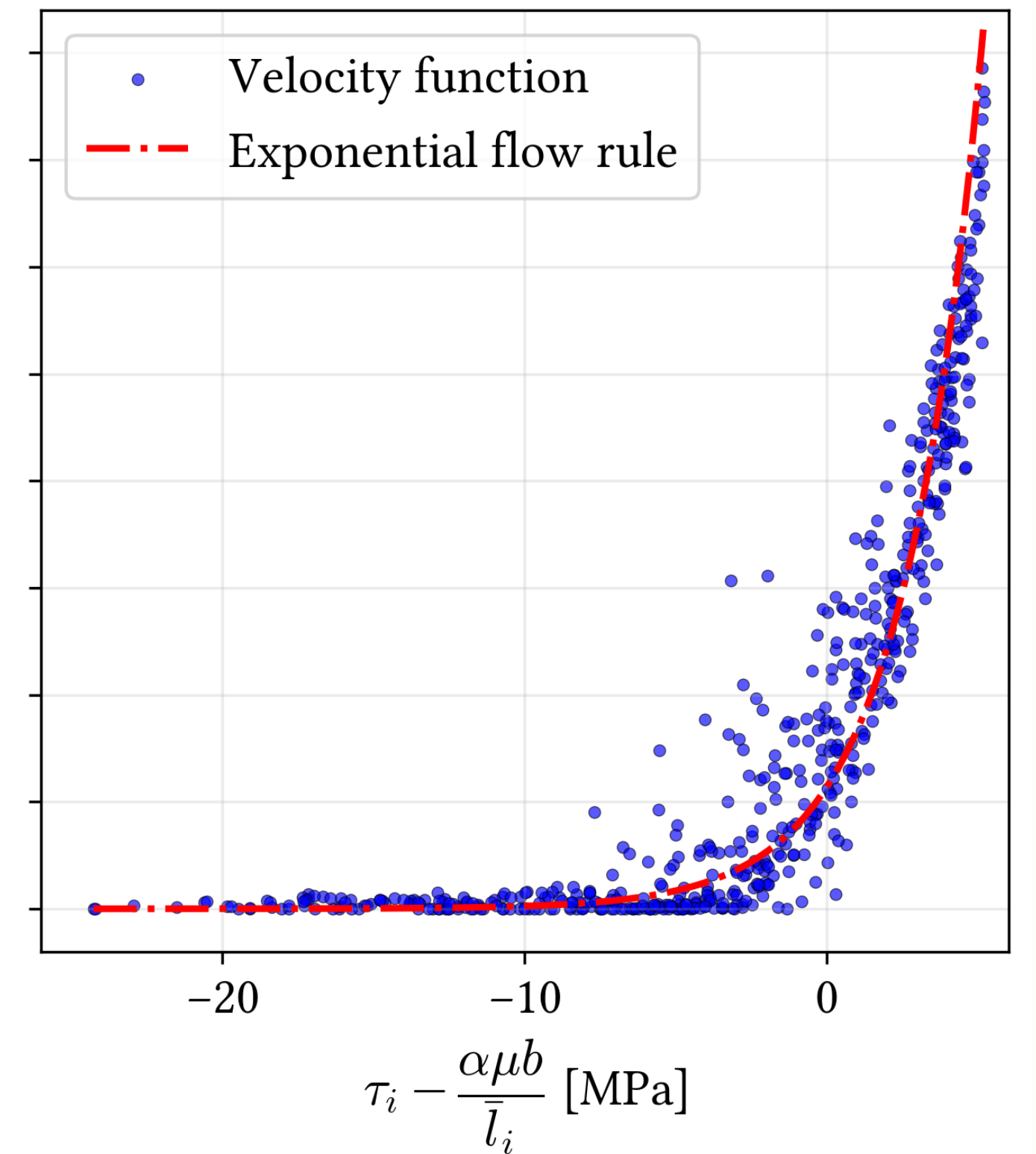
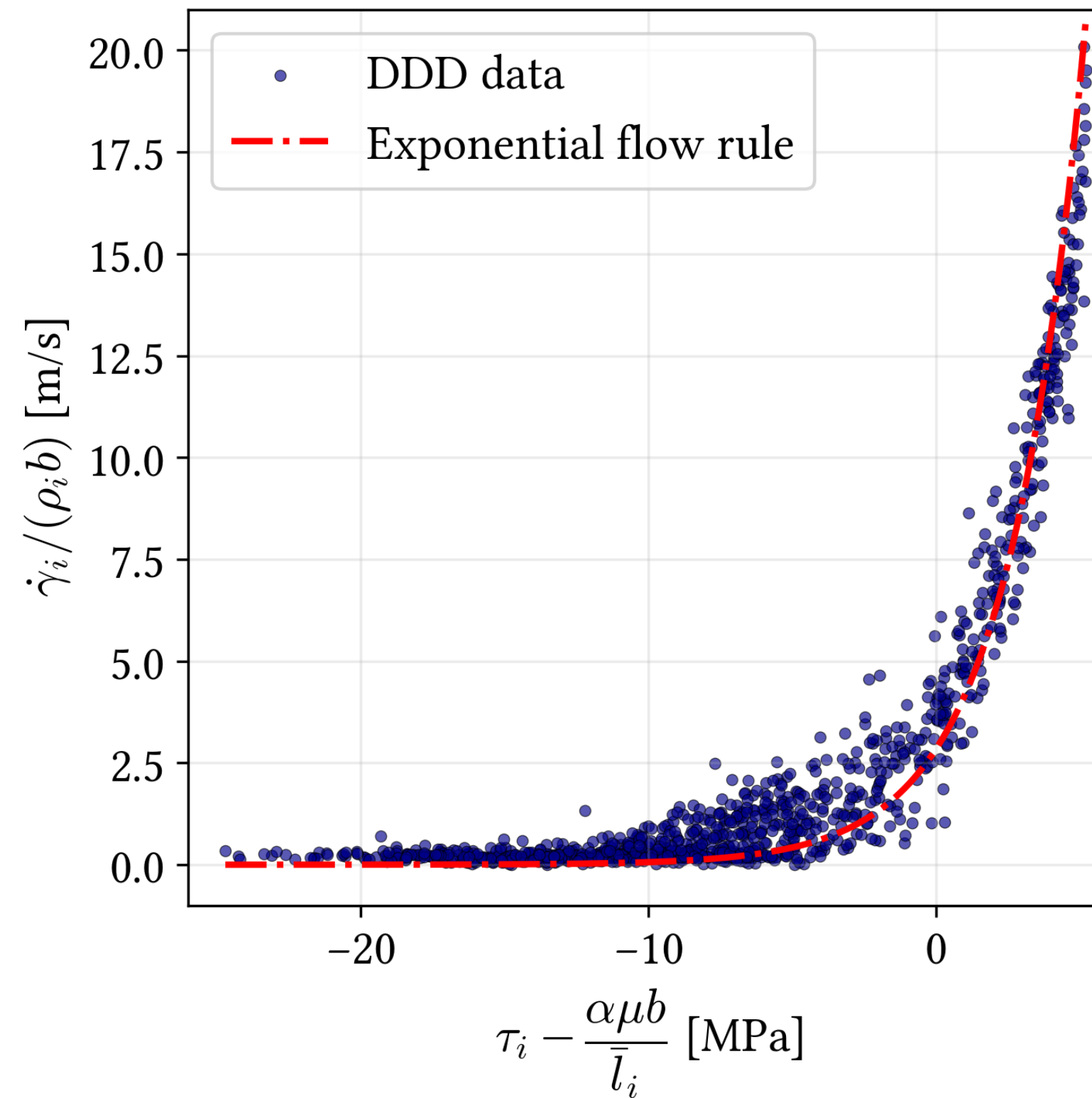
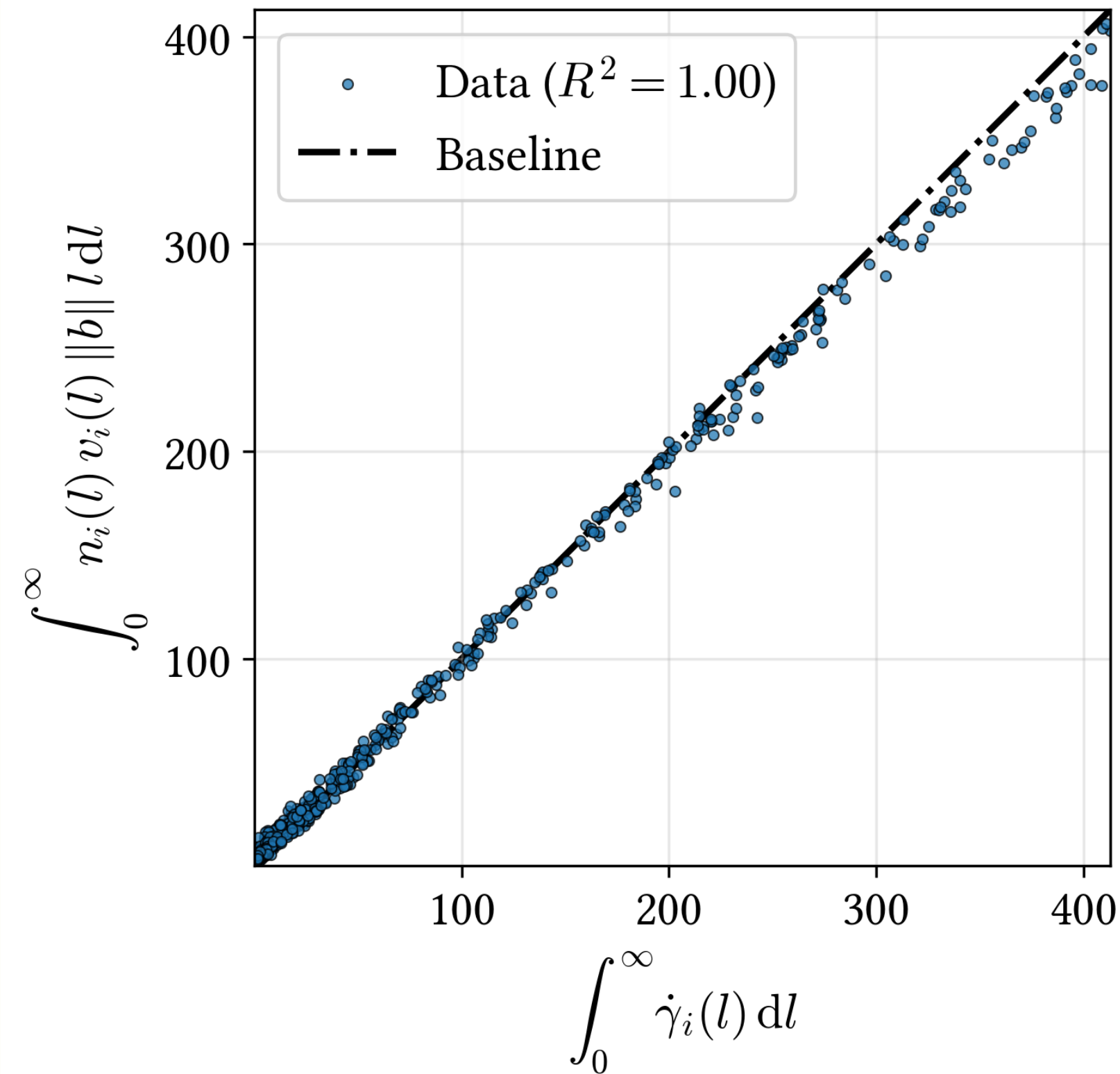
We postulate that this velocity function takes the form a sigmoid function.

This function captures an asymptotic behavior and “activation effects” w.r.t. link length.

Flow rule from link statistics

Previous work reported density-based flow rule
(Akhondzadeh et al., *JMPS*, 2020):

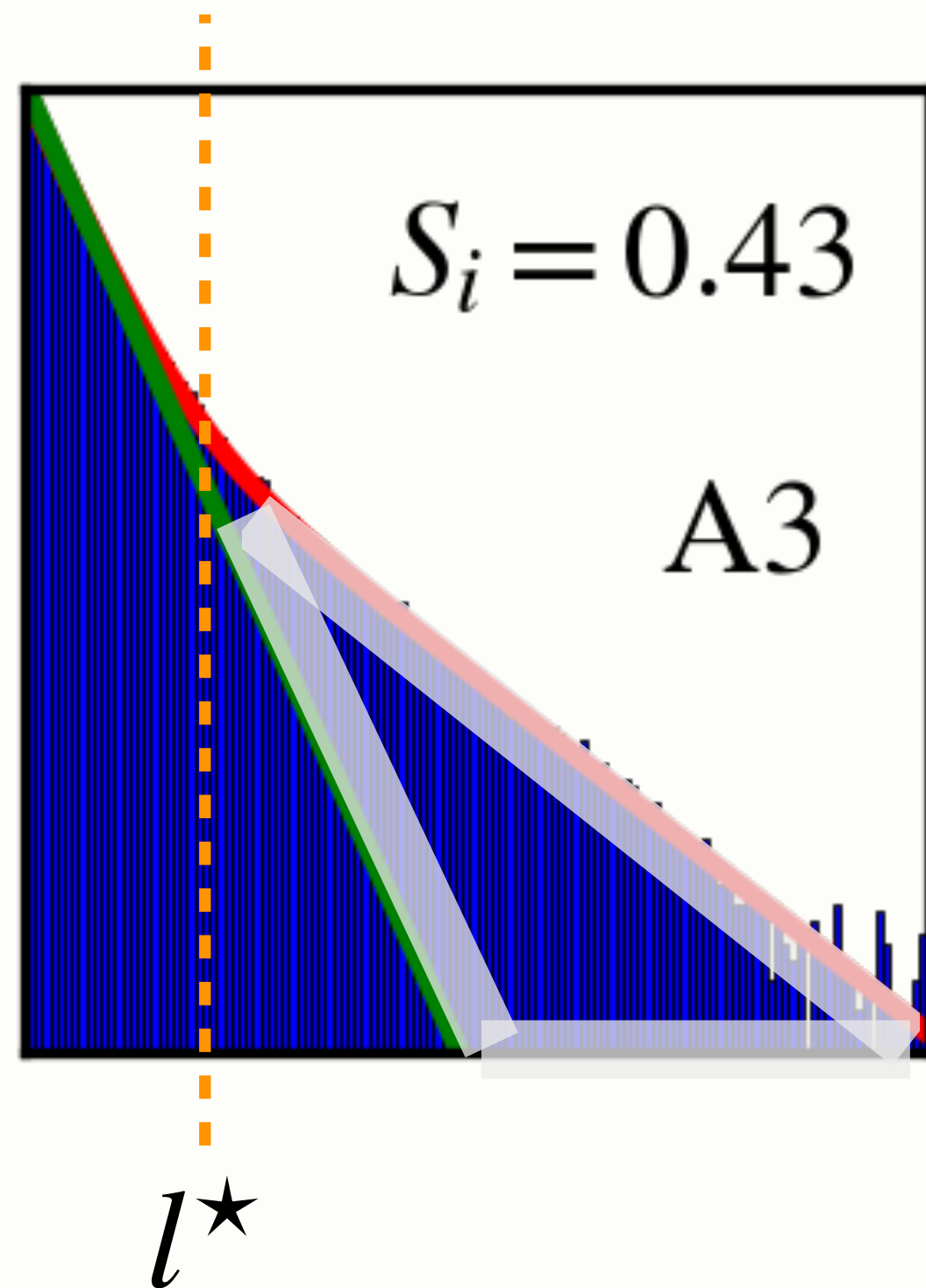
$$\frac{\dot{\gamma}_i}{\rho_i b} = v_0 \exp \left[\frac{1}{s_0} \left(\tau_i - \left(\mu b \sqrt{a'_{ij} \rho_j} - \tau_0 \right) \right) \right]$$



The proposed model can predict the overall strain rates pretty accurately. It also captures the spread of the shear rates when plotted against the applied stress.

Statistical characteristics of long links

Statistical characteristics



“Transition length” from single \rightarrow double exponential distribution:

$$l^* = \ln \left(\frac{N_i^{(1)}}{l_i^{(1)}} \cdot \frac{l_i^{(2)}}{N_i^{(2)}} \right) / \left(\frac{1}{l_i^{(1)}} - \frac{1}{l_i^{(2)}} \right)$$

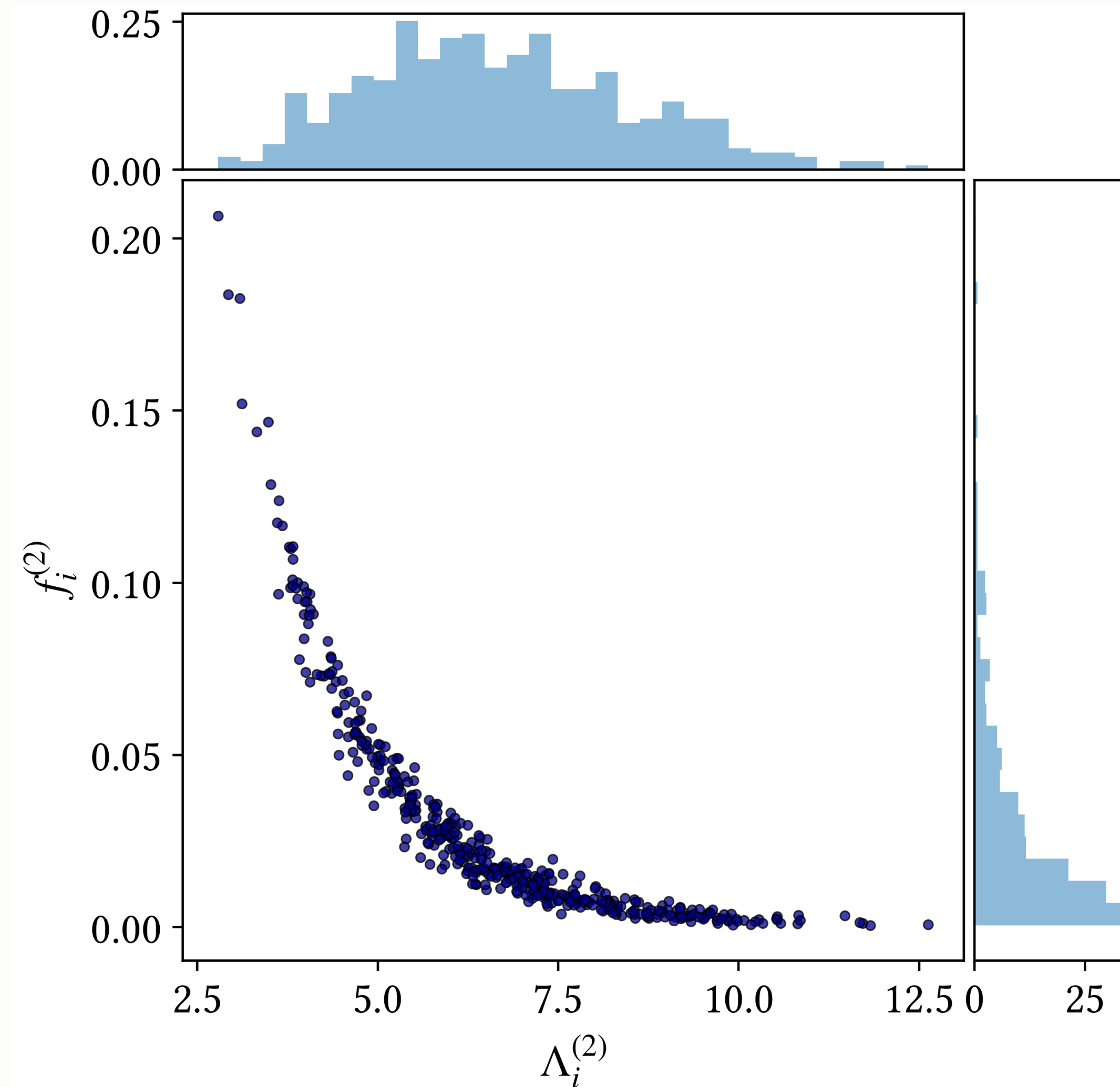
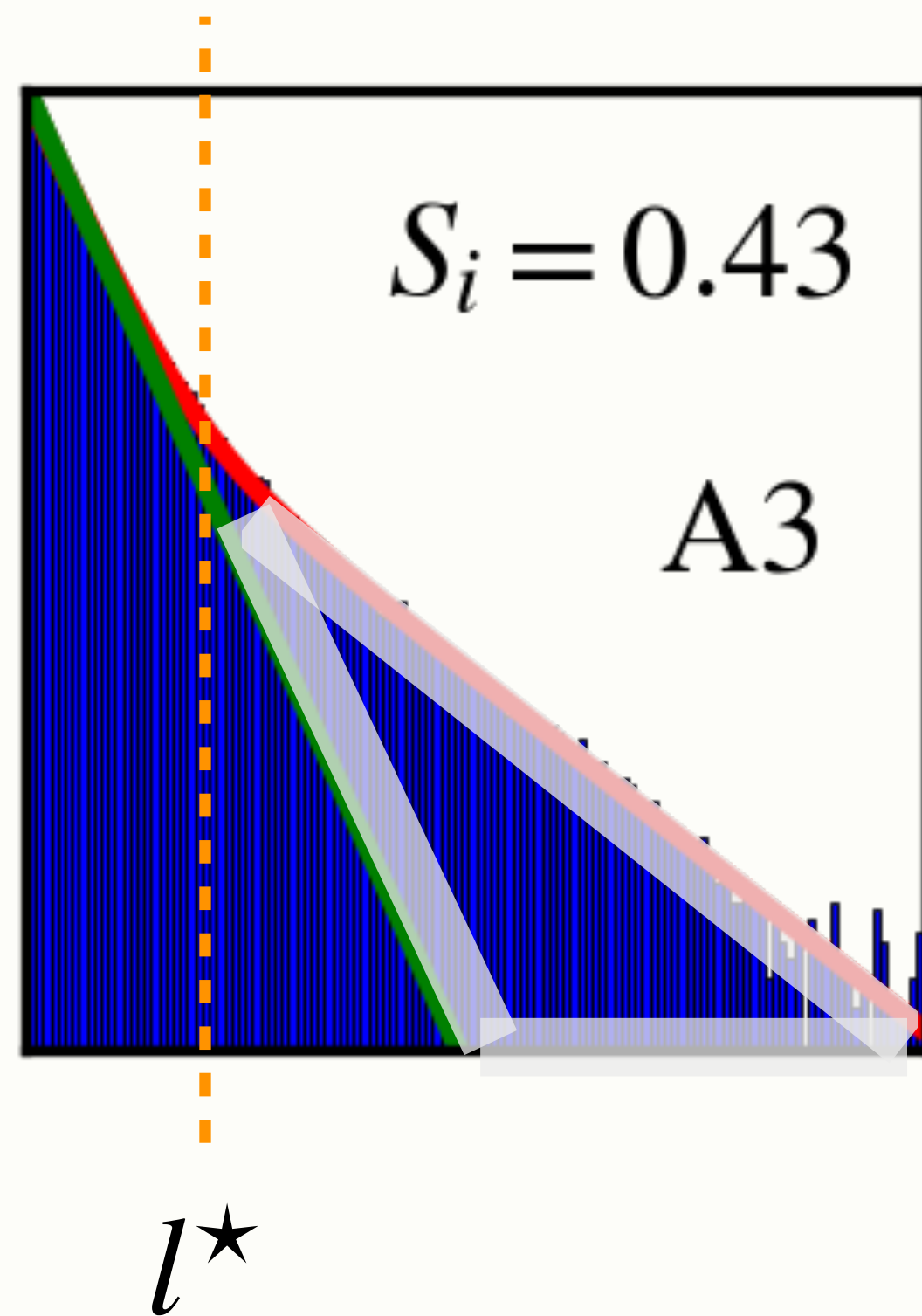
Fraction of longer links (2nd exponential) in the full distribution:

$$f_i^{(2)} \equiv \frac{1}{N_i} \int_{l^*}^{\infty} \frac{N_i^{(2)}}{\bar{l}_i^{(2)}} e^{-l/\bar{l}_i^{(2)}} dl$$

Average link length of the tail (of the 2nd exponential):

$$\Lambda_i^{(2)} \equiv \frac{1}{\bar{l}_i} \frac{1}{f_i^{(2)} N_i} \int_{l^*}^{\infty} l \frac{N_i^{(2)}}{\bar{l}_i^{(2)}} e^{-l/\bar{l}_i^{(2)}} dl = \frac{l^* + \bar{l}_i^{(2)}}{\bar{l}_i} = \frac{l^*}{\bar{l}_i} + \lambda_i^{(2)} = \lambda_i^{(2)} \left(1 + \frac{l^*}{\bar{l}_i^{(2)}} \right).$$

Statistical characteristics



Long-tail links typically constitute less than 5% of all links but are 5–10 times longer than the system average \bar{l}_i , with a clear negative correlation between tail fraction $f_i^{(2)}$ and characteristic length $\Lambda_i^{(2)}$.

Double exponential distributions

Single exponential distribution
(no fitting parameters):

$$n_i(l) = \frac{N_i}{\bar{l}_i} e^{-l/\bar{l}_i}$$

Double exponential distribution (summation
of two exponential distributions):

$$n_i(l) = \frac{N_i^{(1)}}{\bar{l}_i^{(1)}} e^{-l/\bar{l}_i^{(1)}} + \frac{N_i^{(2)}}{\bar{l}_i^{(2)}} e^{-l/\bar{l}_i^{(2)}}$$

Fitting parameters (for the
double exponentials):

$$\lambda_i^{(1)} \equiv \bar{l}_i^{(1)} / \bar{l}_i$$

$$\lambda_i^{(2)} \equiv \bar{l}_i^{(2)} / \bar{l}_i$$

Fitting constrains (for the
double exponentials):

$$N_i^{(1)} + N_i^{(2)} = N_i$$

$$N_i^{(1)} \bar{l}_i^{(1)} + N_i^{(2)} \bar{l}_i^{(2)} = N_i \bar{l}_i$$

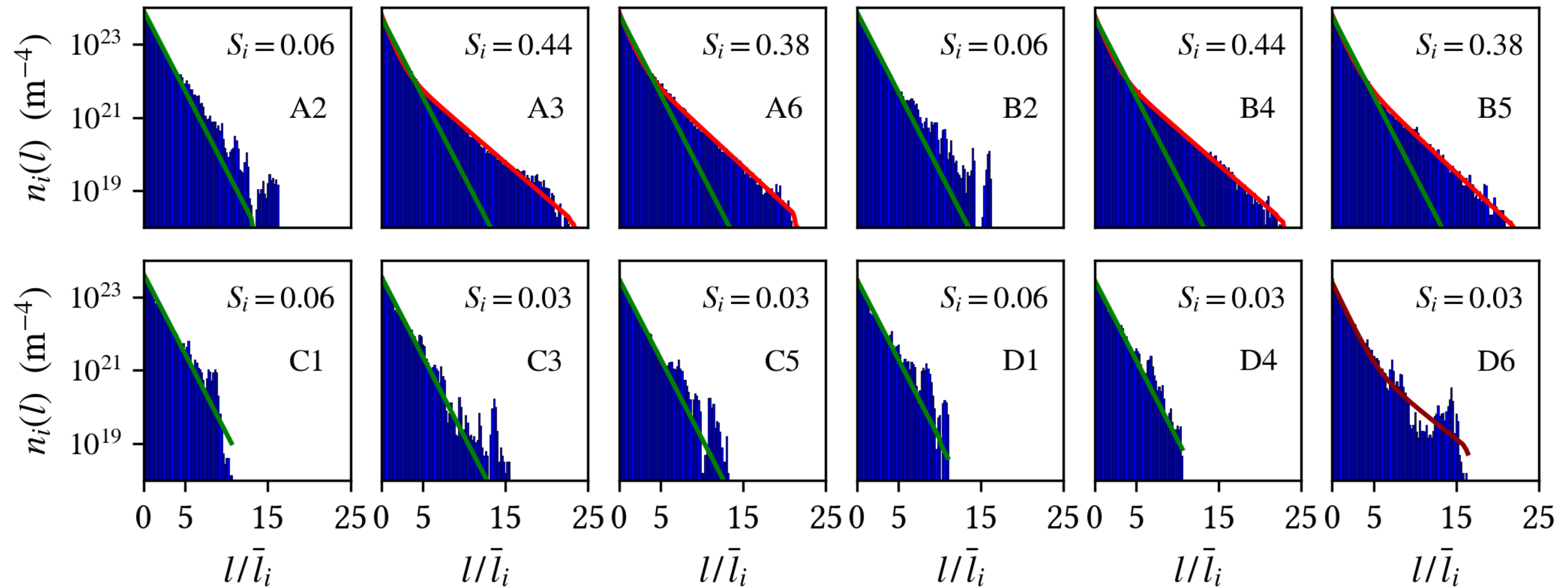
Double exponential distributions

Index i	\mathbf{n}_i	\mathbf{b}_i	SB index	S_i	N_i	$N_i^{(1)}$	$N_i^{(2)}$	\bar{l}_i	$\lambda_i^{(1)}$	$\lambda_i^{(2)}$	ρ_i
1	($\bar{1}11$)	$\frac{1}{2}[0\bar{1}1]$	A2	0.40	4.15	3.89	0.26	4.53	0.91	2.42	1.88
2	($\bar{1}11$)	$\frac{1}{2}[101]$	A3	0.43	5.64	5.15	0.48	5.32	0.86	2.44	3.00
3	($\bar{1}11$)	$\frac{1}{2}[110]$	A6	0.03	4.17	—	—	3.94	—	—	1.64
4	(111)	$\frac{1}{2}[0\bar{1}1]$	B2	0.42	5.06	4.83	0.23	5.43	0.90	3.13	2.75
5	(111)	$\frac{1}{2}[\bar{1}01]$	B4	0.43	4.95	4.57	0.37	5.16	0.87	2.55	2.55
6	(111)	$\frac{1}{2}[\bar{1}10]$	B5	0.01	3.83	—	—	4.26	—	—	1.63
7	($\bar{1}11$)	$\frac{1}{2}[011]$	C1	0.39	4.86	4.74	0.12	4.63	0.95	3.01	2.25
8	($\bar{1}11$)	$\frac{1}{2}[101]$	C3	0.38	4.25	3.94	0.31	4.29	0.88	2.48	1.83
9	($\bar{1}11$)	$\frac{1}{2}[110]$	C5	0.01	3.72	—	—	4.01	—	—	1.49
10	($\bar{1}11$)	$\frac{1}{2}[011]$	D1	0.42	5.38	4.87	0.50	5.17	0.85	2.50	2.78
11	($\bar{1}11$)	$\frac{1}{2}[\bar{1}01]$	D4	0.38	4.57	4.16	0.40	4.68	0.87	2.35	2.14
12	($\bar{1}11$)	$\frac{1}{2}[110]$	D6	0.03	3.89	—	—	3.88	—	—	1.51

Loading orientation: [0.03, 0.05, 0.99]

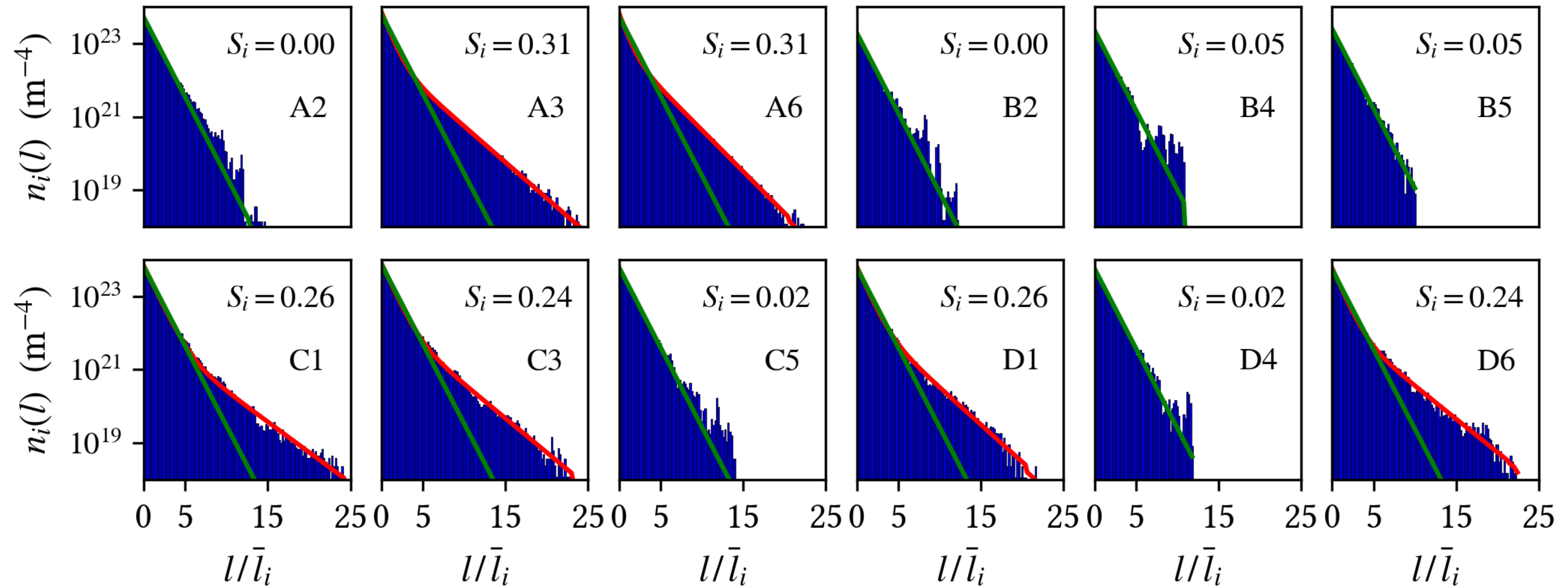
The first exponential takes up most of the links in the distribution.

Link statistics near [0 1 1]



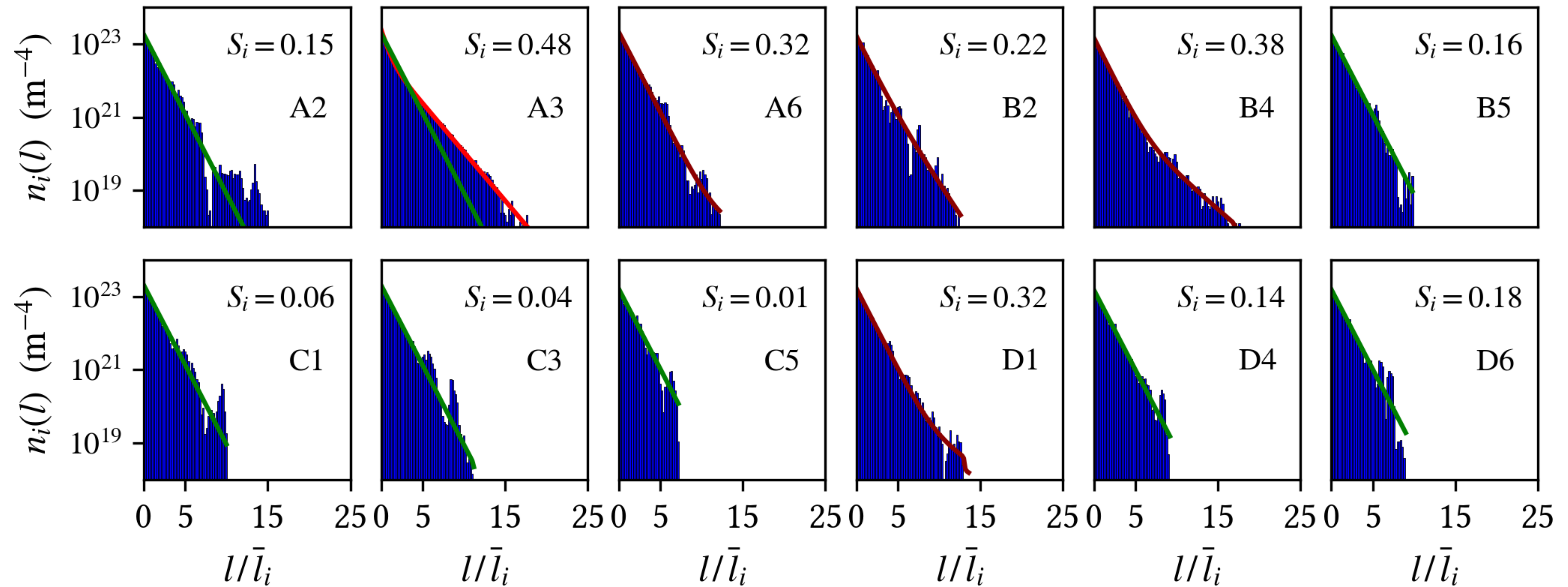
Loading orientation: [0.00, 0.65, 0.76]

Link statistics near [1 1 1]



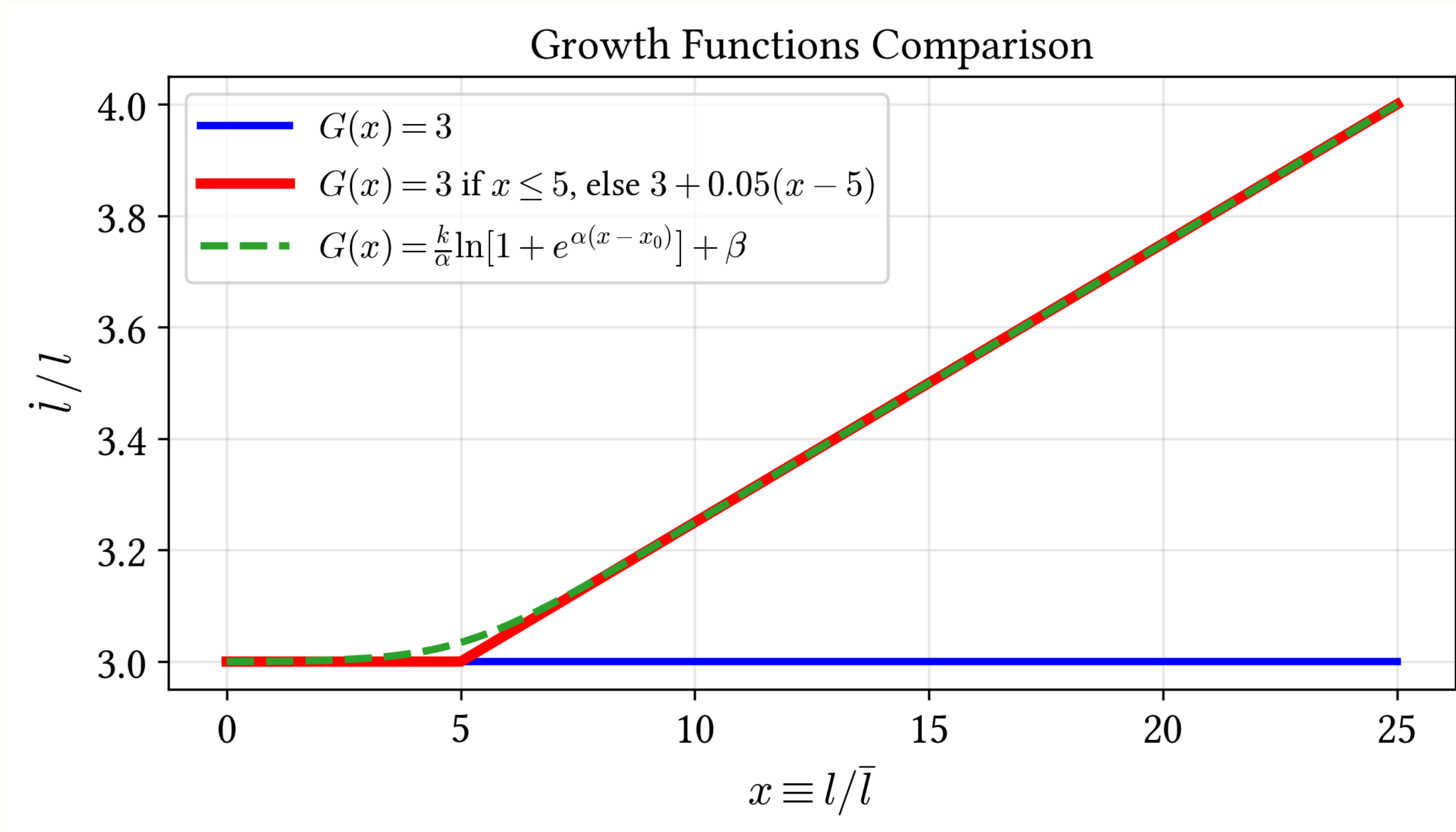
Loading orientation: [0.53, 0.60, 0.60]

Link statistics near [1 2 3]



Loading orientation: [0.24, 0.49, 0.84]

Growth function comparison



Doesn't have to be a bistep function!